



Massachusetts Institute of Technology



Plasma Science & Fusion Center

The Case for High Field Fusion (abridged)

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available at firefusionpower.org*

psfc.mit.edu



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Case: The high magnetic field path is optimal to obtain our absolute science and energy goals

- From plasma science viewpoint there are no serious “tradeoffs” in the design of your MFE burn/energy mission, you always maximize B field strength
- Achieving high B field with electromagnets has fundamental *science* limits; understanding this evolving science allows us as plasma physicists how to best meet our science and energy missions

Why now?

- **15+ years since we talked about this.. many of our younger scientists don't recall key features of debate about the “tactics” involved in achieving burning plasmas.**
- **And haven't things changed meanwhile?**
 - **In physics of plasmas, magnets, etc.**
 - **Or maybe we just have more experience & insight**

Volumetric fusion power density

$$\beta \equiv \frac{P_{th}}{P_{magnetic}} = \frac{P_{th}}{B^2 / 2\mu_o}$$

Troyon limit (tokamaks)

$$\beta_N = \frac{\beta q}{5\epsilon S(\kappa)}$$

Troyon, Gruber Phys. Lett. 110A (1985)

+

$$P_f \approx 8 P_{th}^2$$



Generic

$$P_f \sim \beta^2 B^4$$

Tokamak

$$P_f \sim \frac{\beta_N^2 \epsilon^2 S(\kappa) B^4}{q^2}$$

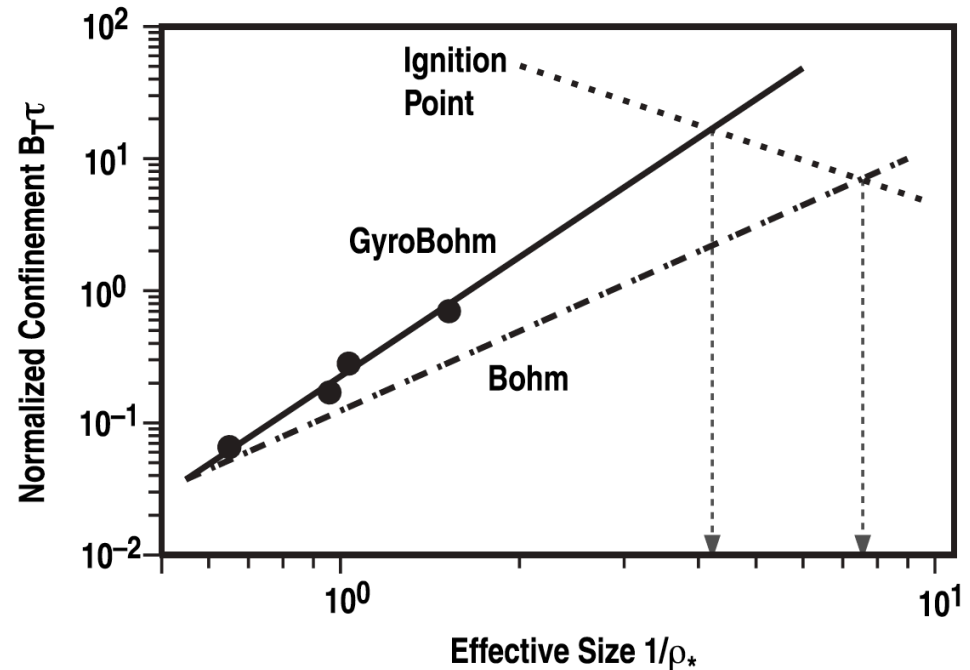
Confinement: tokamak

- Expressing confinement through “wind-tunnel” dimensionless scaling laws

$$B \tau \propto \rho_*^{3.1} \beta^0 \nu^{-0.35} q_{95}^{-1.4} \kappa^{2.2} \quad \text{Petty}$$

Extract R, B at
Fixed R/a

$$\tau \sim R^{3.1} B^{2.1}$$



ITPA
Luce, Petty, Cordey PPCF 50 (2008)

Energy gain at fixed physics & shape parameters

Target

$$P_{th}$$

X

$$\tau_E$$

=

Target

$$P_{th} \tau_E$$

Generic

$$R^2 B^2$$

$$R^2 B^4$$

$$B^2$$

H₉₈

$$R^{2.7} B^{3.5}$$

$$R^{2.7} B^{5.5}$$

Petty

$$R^{3.1} B^{2.1}$$

$$R^{3.1} B^{4.1}$$

ISS04

$$R^{2.8} B^{2.2}$$

$$R^{2.8} B^{4.2}$$

High B (+ strong shaping) enables stationary pedestal with high absolute pressure

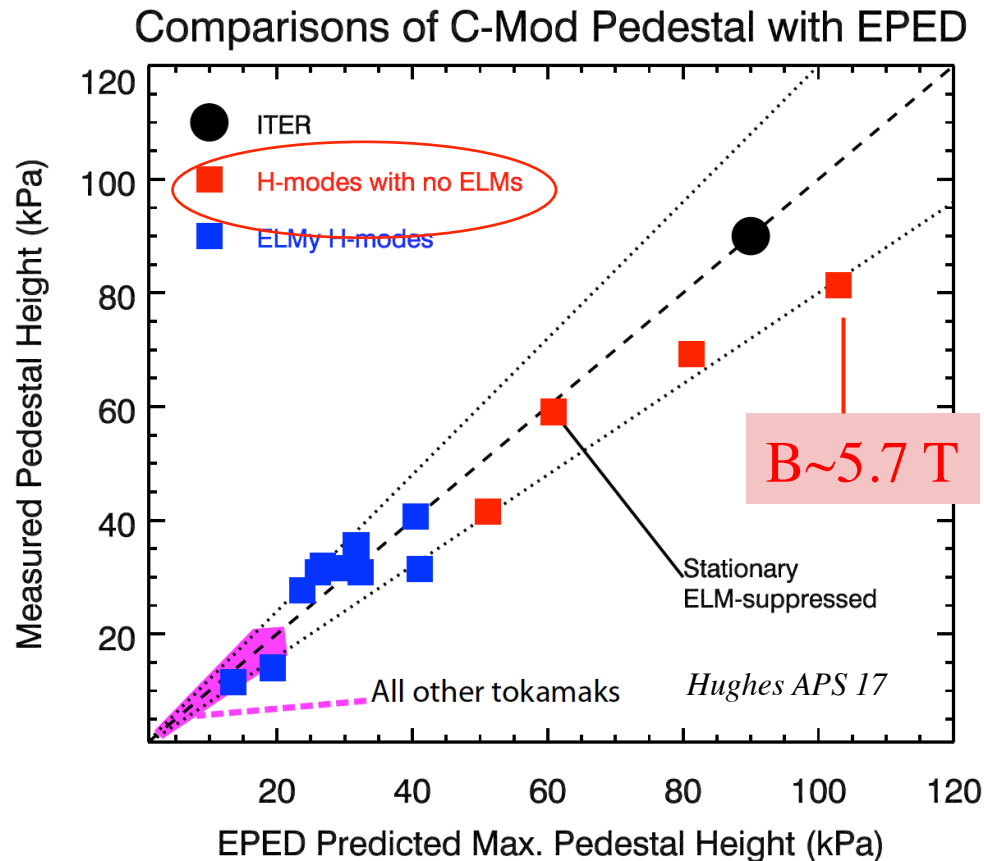
~ Peeling-Ballooning Stability Limit

Snyder et al NF 2011

$$\beta_{N, Ped} \leq \left(\frac{\Delta\psi_{ped}}{5\%} \right)^{3/4}$$

$$\beta_N \sim \frac{p_{ped}}{p_{magnetic}} \frac{q}{\epsilon}$$

$$p_{ped} \leq \left(\frac{\Delta\psi}{5\%} \right)^{3/4} \frac{B^2}{q}$$



Am I happy or sad?

Issue	Scaling	
Power density	B^4	😊
Confinement (generic)	$R^2 B^2$	😊
Confinement (tokamak)	$R^{2.7} B^{3.5}$ (H_{98}) $R^{3.1} B^{2.1}$ (Petty)	😊
Confinement (stellarator)	$R^{2.8} B^{2.1}$	😊
Gain	$R^{2-3.1} B^{4-5.5}$	😊
Stable pedestal/I-mode	$\sim \beta_N B^2$	😊

Issue	Scaling	
Density (tokamak)	$R^{-1} B^1$	😊
Density (stellarator)	$\beta B^{2.5}$ (burning)	😊
Heat exhaust: min. f_Z	$R^{1.3} B^{0.9}$	😊
Heat exhaust: $q//$	B^{-1} (burning)	🤔
Runaway e- amp.	$\exp(R^{0.28} / B^{0.3})$	😊
Synchrotron: runaways	B^2	😊
Synchrotron:thermal	$\sim B^{1.5}$	🤔
TAE	$n \sim B, v_A \sim B$	😊

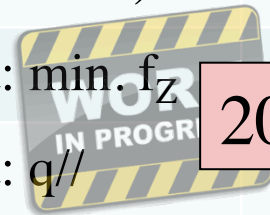


Am I happy or sad? *I'm happier than before*

Issue	Scaling
Power density	B^4
Confinement (generic)	$R^2 B^2$
Confinement (tokamak)	$R^{2.7} B^{2.1}$ (Petty)
	1998
	2008
Confinement (stellarator)	$R^{2.8} B^{2.1}$
	2005
Gain	$R^{2-3.1} B^{4-5.5}$
	2010
Stable pedest	$B_N B^2$
	2016



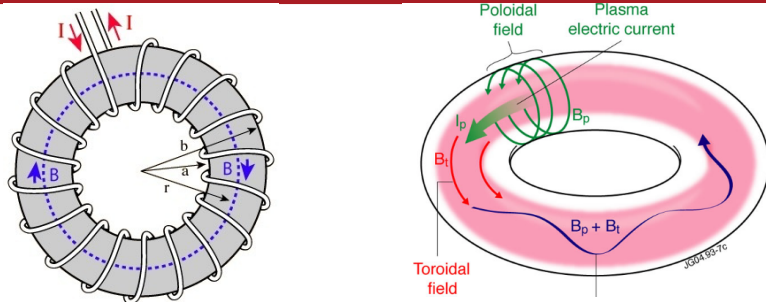
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Synchrotron: runaways	B^2
Synchrotron: thermal	$\sim B^{1.5}$
TAE	$n \sim B, v_A \sim B$



2010-17

2005-17

Electromagnets & Tokamak plasmas: same physics



$$\nabla \times \vec{B} = \mu_0 \vec{j}$$

Ampere's law

$$B \sim j$$

$$\nabla p = \vec{j} \times \vec{B}$$

Force balance

$$P_{magnet} \sim B^2$$

$$P = \eta j^2$$

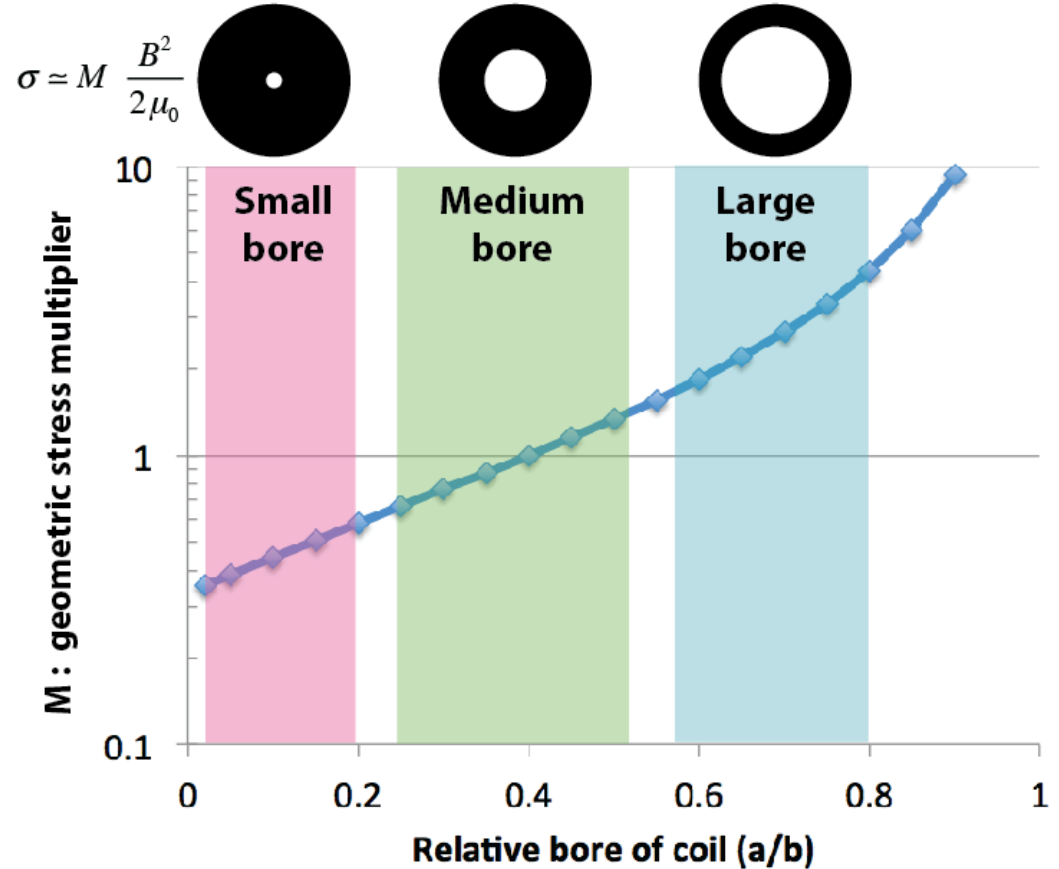
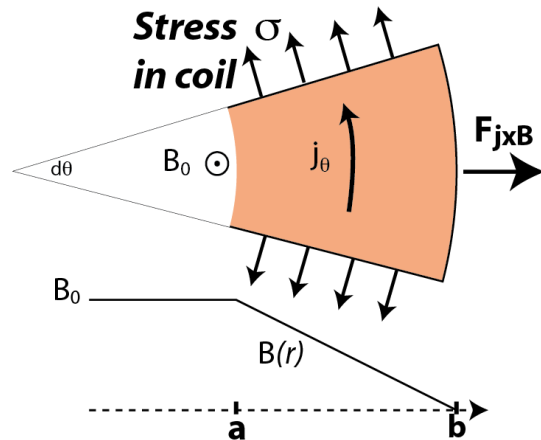
Ohmic heating

$$P_{magnet} \sim B^2$$

As in toroidal plasma physics, aspect ratio is a critical and complex optimization

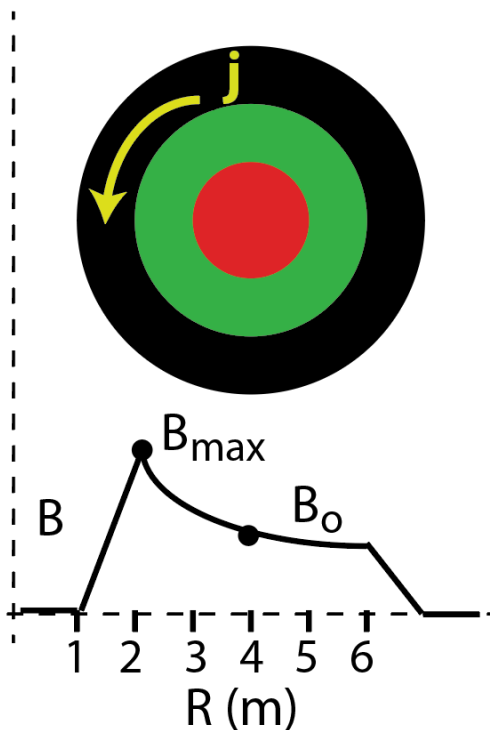
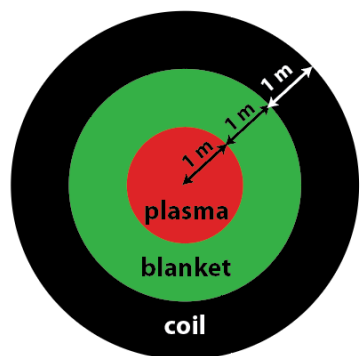
$$x \equiv \frac{a}{b}$$

$$M = \frac{2x + 1}{3(1 - x)}$$



Simple toroidal “solenoid” to explore limits

$$R=4 \text{ m}, A=4, B_0=B_{\text{max}}/2$$



$$B = \frac{\mu_0 \int j_z \pi R dR}{2\pi R}$$

$$B_{\text{max}} = 0.3\pi j_{MA/m^2}$$

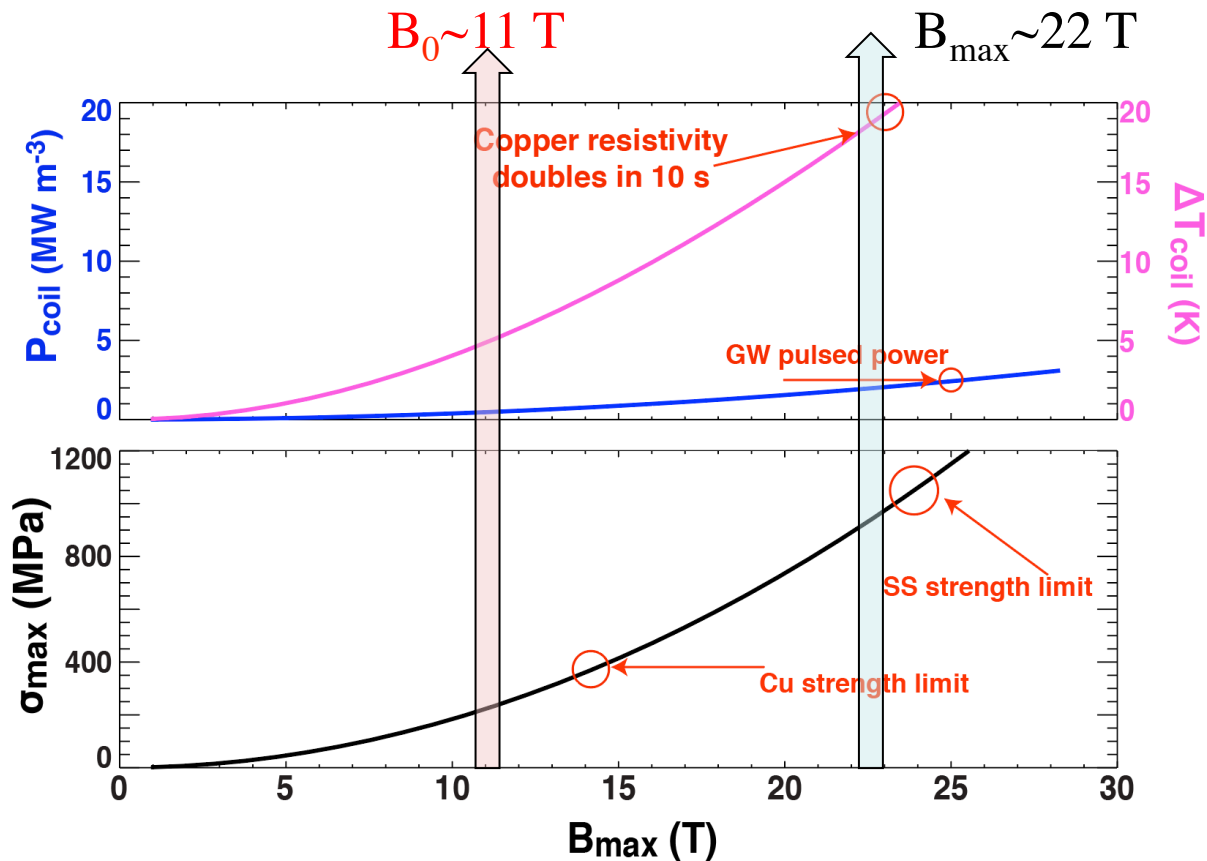
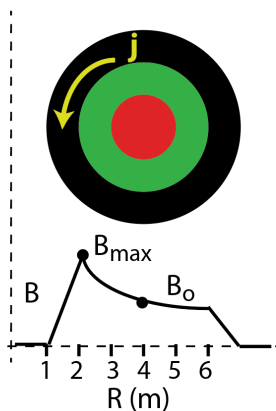
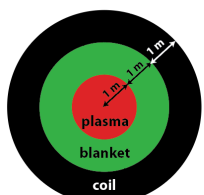
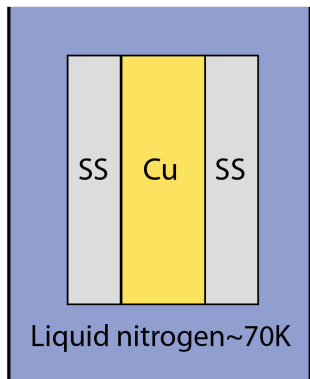
$$x \equiv \frac{a}{b} = \frac{2}{3}$$

$$M = 2.3$$

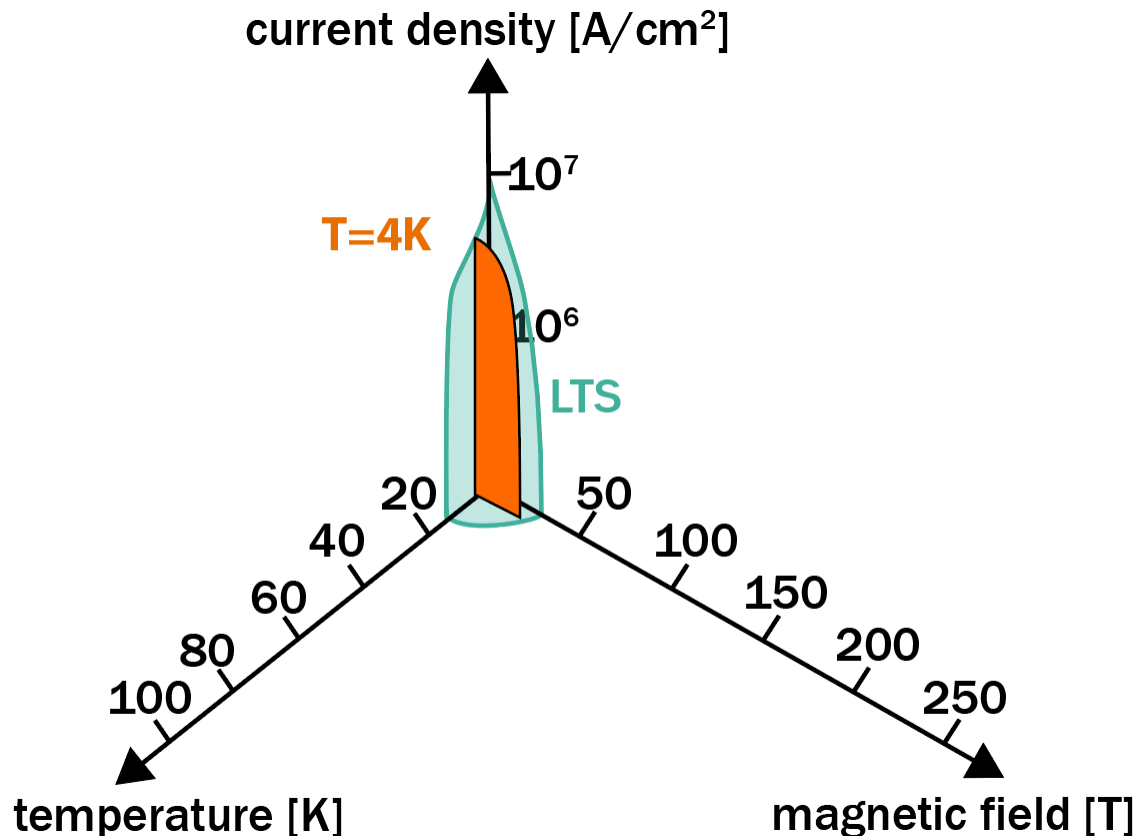
$$\sigma_{\text{max}} [MPa] \approx M \frac{B_{\text{max}}^2}{2\mu_0}$$

LN-cooled copper + steel for stress loading

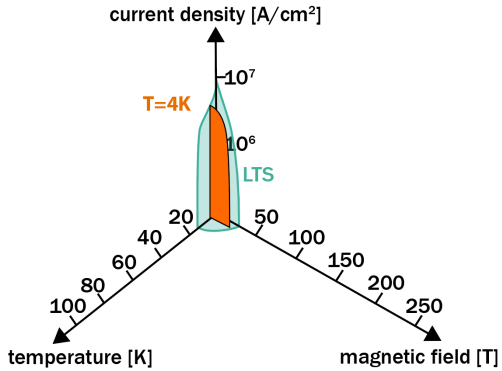
Pulsed due to lack of active cooling



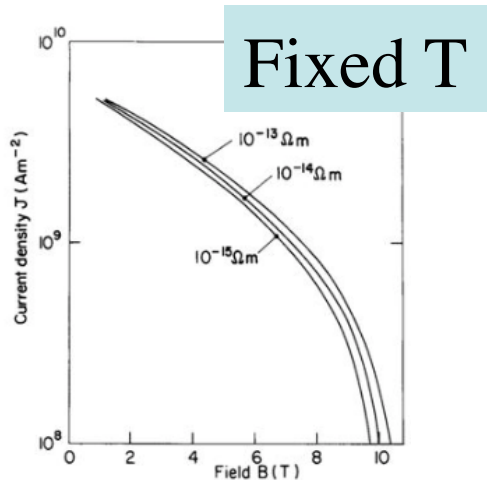
Superconductors: zero resistivity, but a restricted operating space in T, j and B



Superconductors: critical current, at fixed T, depends on SC type and B



$$\frac{J_c}{J_{c,0}} = \left(\frac{B}{B_0} \right)^{-\alpha}$$

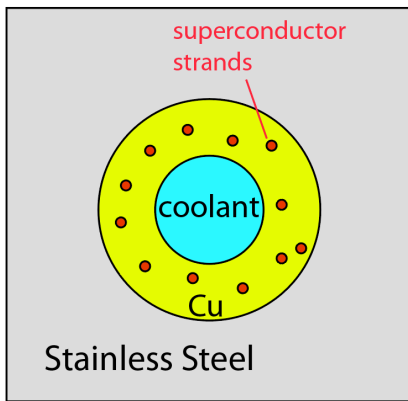


	J_{c0}	B_0	α
Nb-Ti	10 ³	5	3
Nb ₃ -Sn	10 ³	10	3

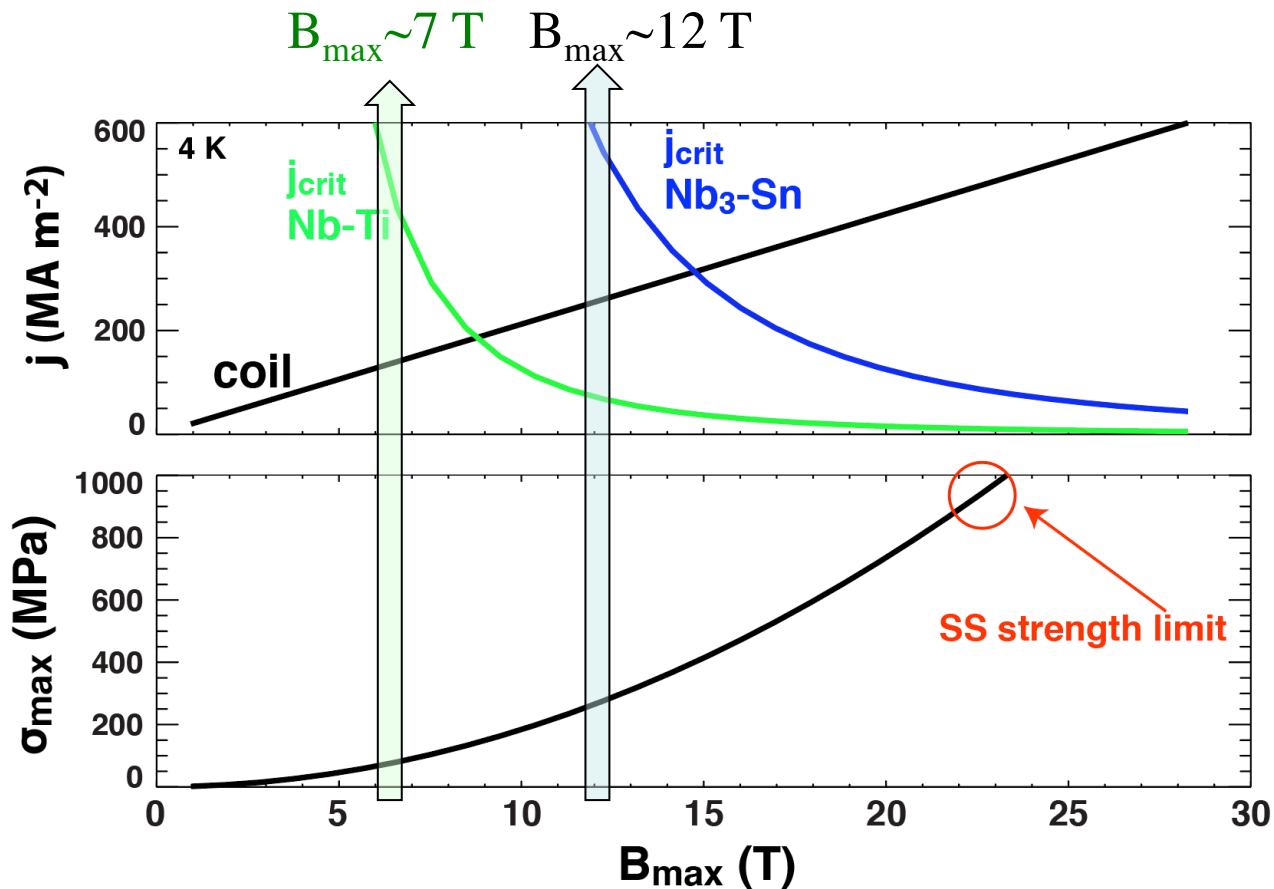
$T \sim 4 \text{ K}, B > B_0$

Nb-Sn superconductors: B limited by critical current at $T \sim 4\text{K}$

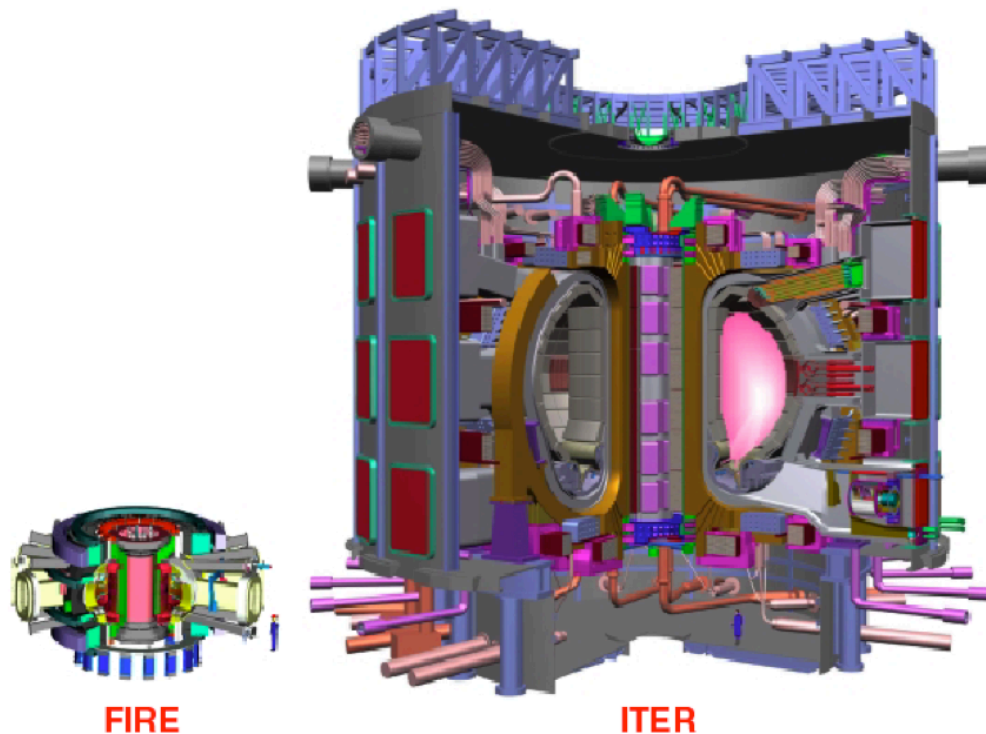
Coil Cross-section



50% SS
22% cool
25% Cu
3% SC



NAS study: Cryogenic Cu could study burning plasma science at 25x smaller volume than Nb₃Sn



$$P_{th} \tau_E \sim R^{2.7} B^{5.5}$$

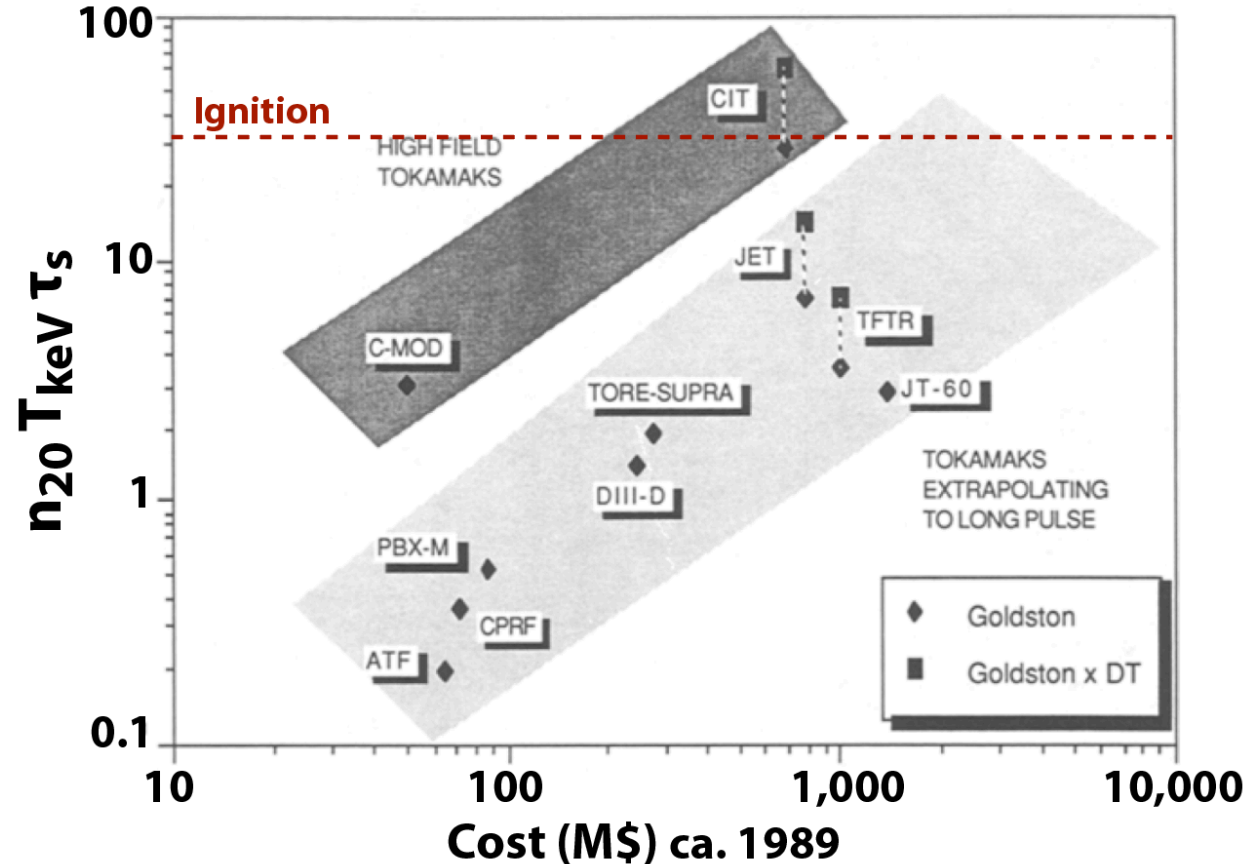
$$\text{Volume} \sim R^3 \sim 1/B^5$$

	FIRE	ITER
B (T)	10	5.3
R (m)	2.14	6.2
Q	10	10
τ / τ_{CR}	> 1	> 1
V_p (m³)	30	800

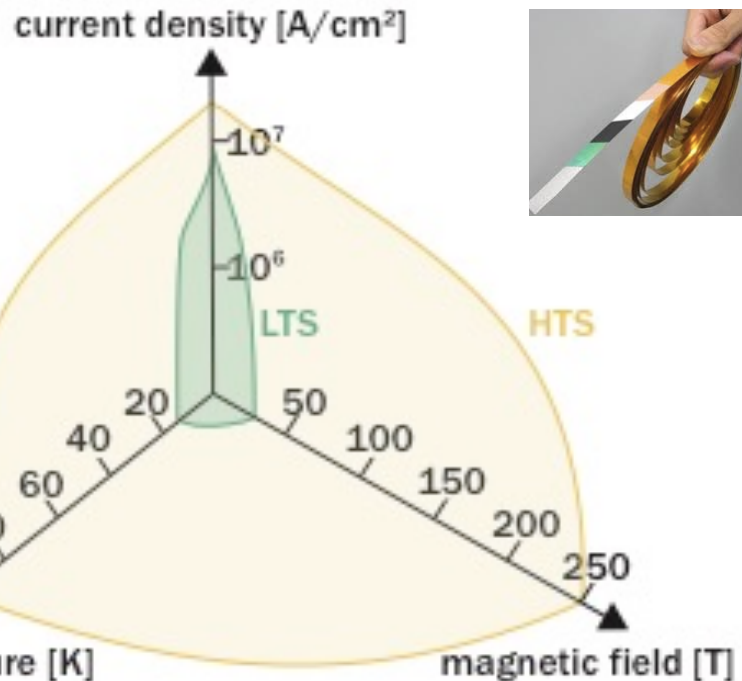
→
25x

Tactics? High-B, compact was known to have ~10-fold performance to cost ca. 1990 but pulsed

Compact Tokamak
Ignition Concepts
J. Willis
J. Fusion Energy 1989



High-Temperature (HTS) REBCO superconductors

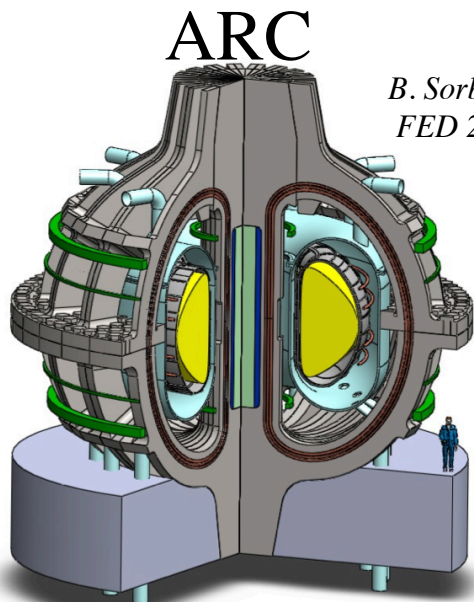


$$\frac{J_c}{J_{c,0}} = \left(\frac{B}{B_0} \right)^{-\alpha}$$

	J_{c0}	B_0	α
Nb-Ti	10^3	5	3
Nb ₃ -Sn	10^3	10	3
REBCO	2.5×10^3	5	0.6

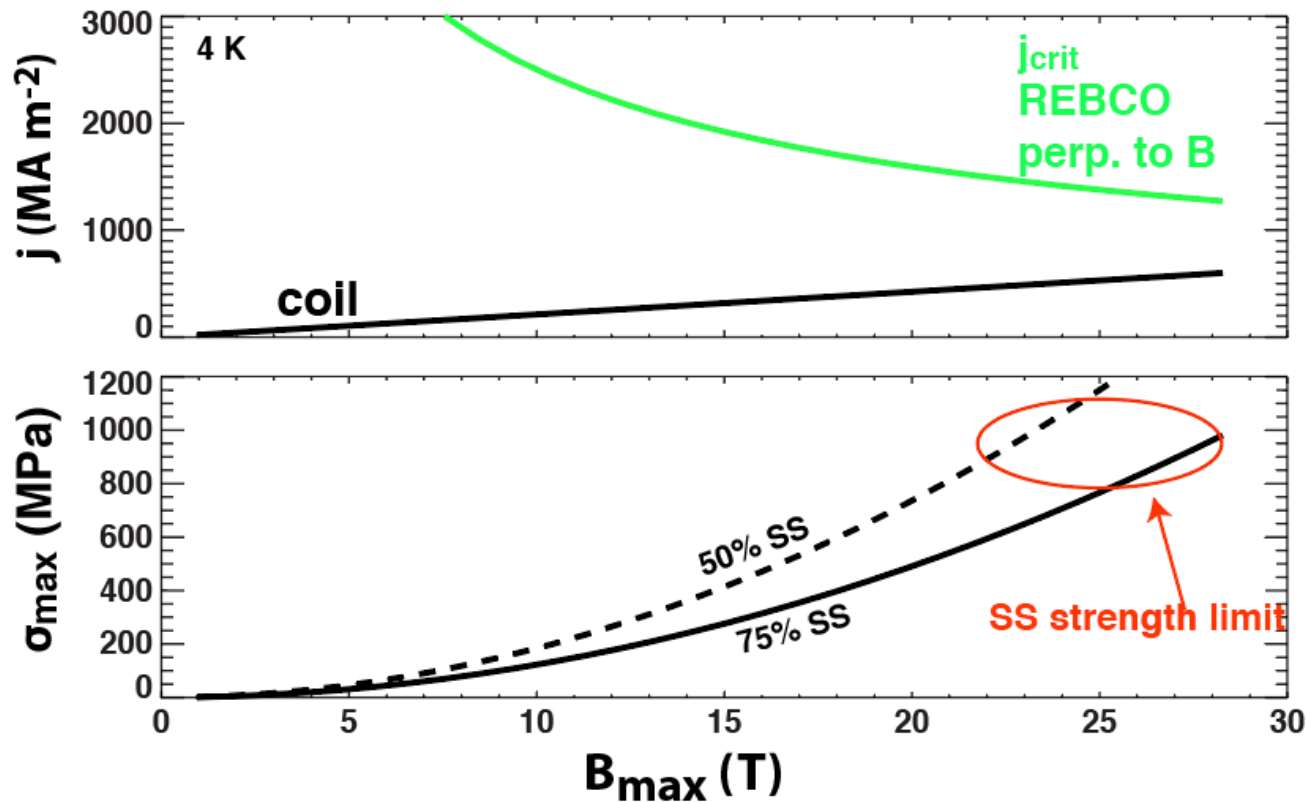
$T \sim 4 \text{ K}, B > B_0$

With HTS magnets, stress is the only limit \rightarrow multiple design choices to achieve $B_{\max} > 20\text{T}$



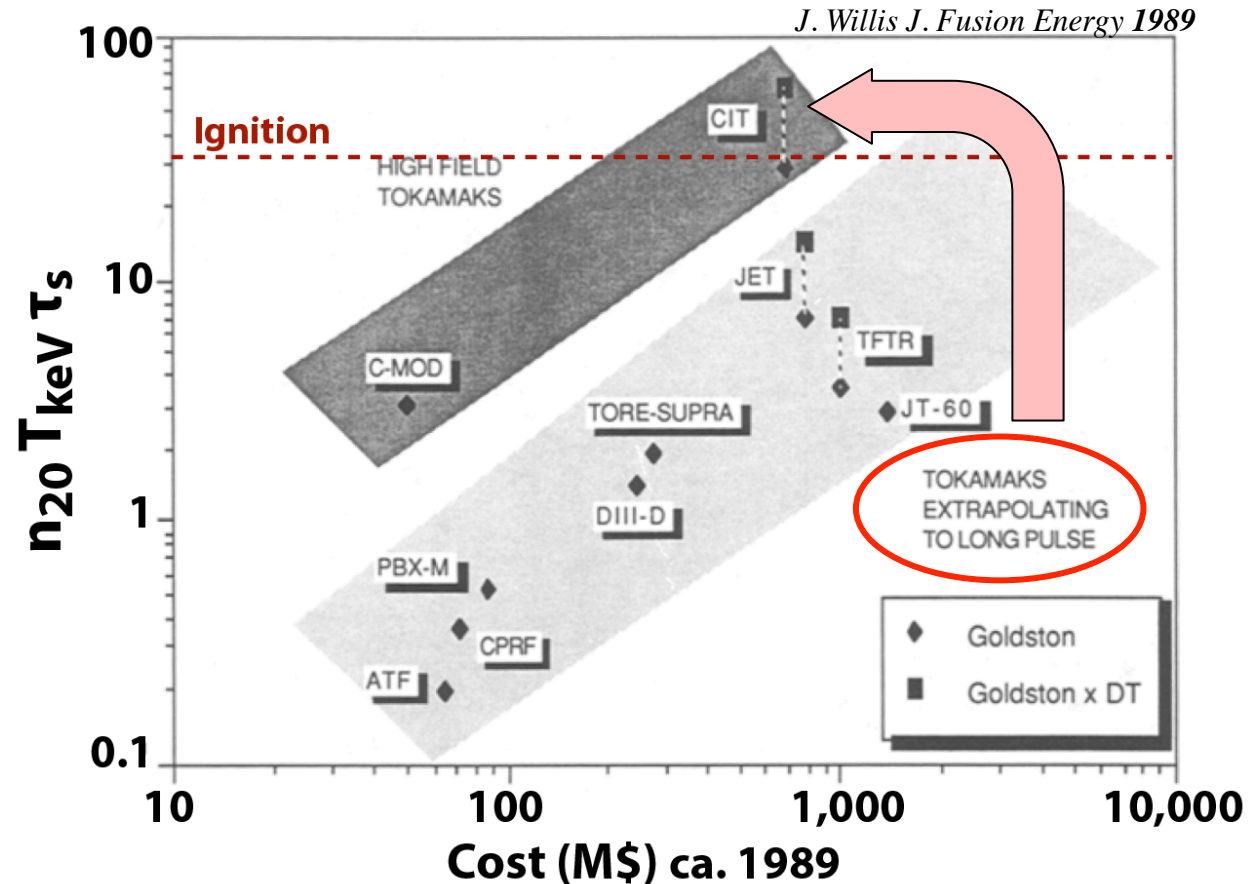
*B. Sorbom et al
FED 2015*

$B_{\max} \sim 23\text{T}$
 $B_0 \sim 9.2\text{T}$
 $\sigma_{\max} \sim 700\text{ MPa}$



HTS magnets clearly change the tactical landscape for magnetic fusion

- ✓ Diversification
- ✓ Risk distribution
- ✓ Speed



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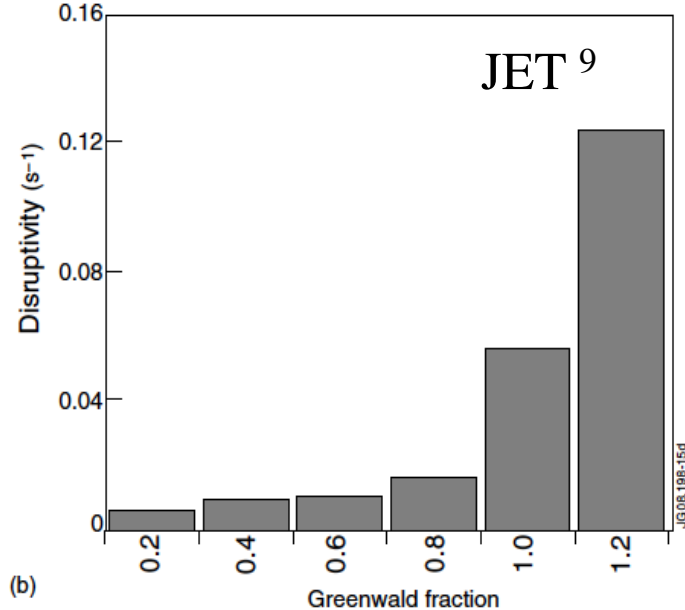
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Density: tokamak

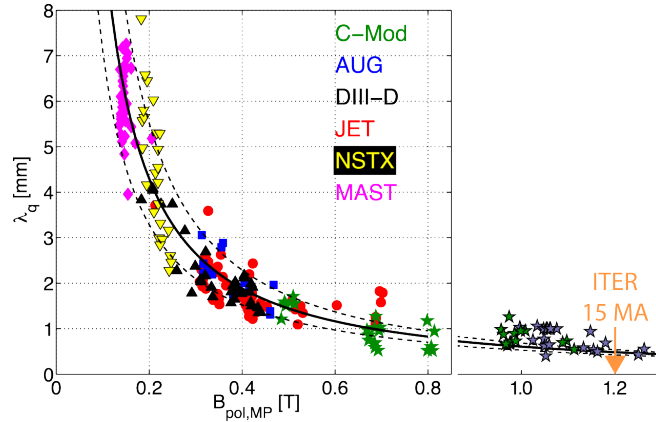
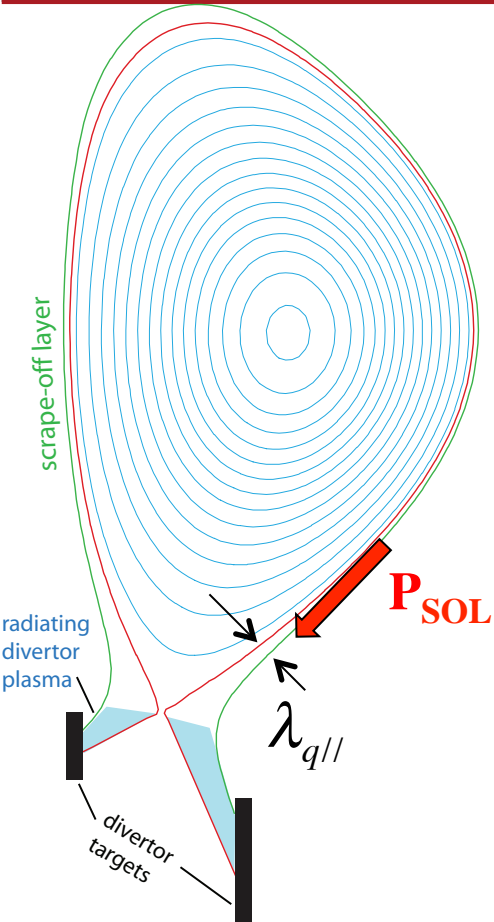
Empirical Greenwald density
is a disruptive limit in tokamaks



De Vries, et al. *Nucl. Fusion* **49** (2009)

$$n \leq n_{Gr} = \frac{I_p}{\pi a^2} \propto \frac{S(\kappa) B}{q R}$$

Power exhaust: tokamak divertor Solutions



$$\lambda_{q||} \propto \epsilon \rho_{pol} \sim 1 / B_{poloidal}$$

$$q_{||} \propto P_{SOL} B / R$$

$$P_{rad} \sim n_{div}^2 f_z F(T_e)$$

$$n_{div} \sim n_{core}^2$$

$$n_{core} \propto \frac{S(\kappa) B}{\epsilon R}$$

Required impurity
Fraction to Detach¹

$$c_Z \propto \frac{P_{SOL}}{B_p f_{Gr}^2}$$

Required impurity
Fraction to Dissipate
Psol in H-mode²

$$f_z \sim B^{0.9} R^{1.3}$$

²M.L. Reinke. Nucl. Fusion 57 (2017)

¹Goldston et al PPCF 2017, APS17