



High fusion performance at high T_i/T_e in JET-ILW baseline plasmas with high NBI heating power and low gas puffing

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JET

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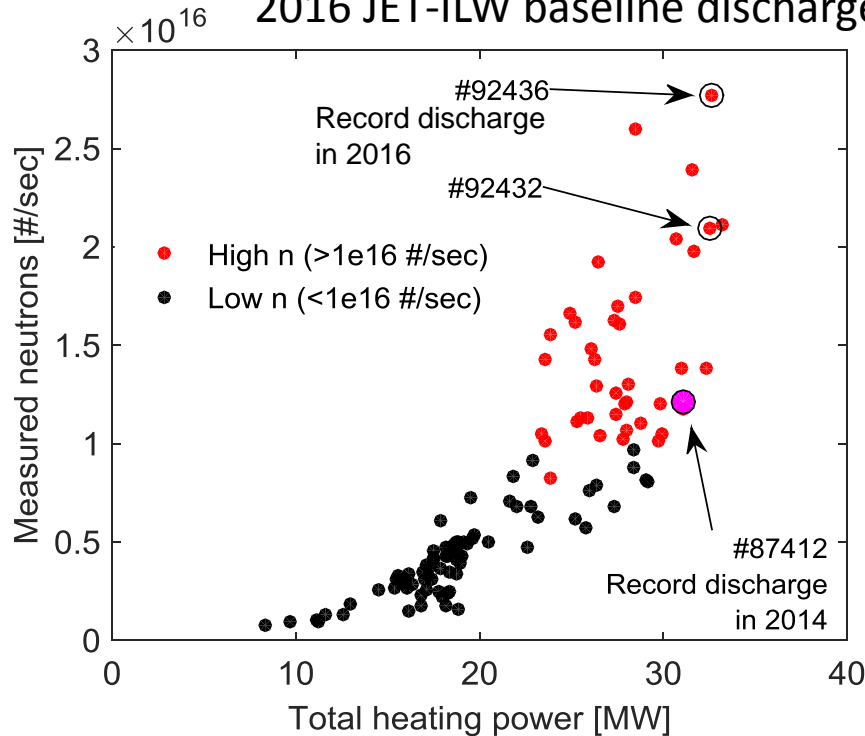


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Key questions on 2016 JET-ILW baseline discharges

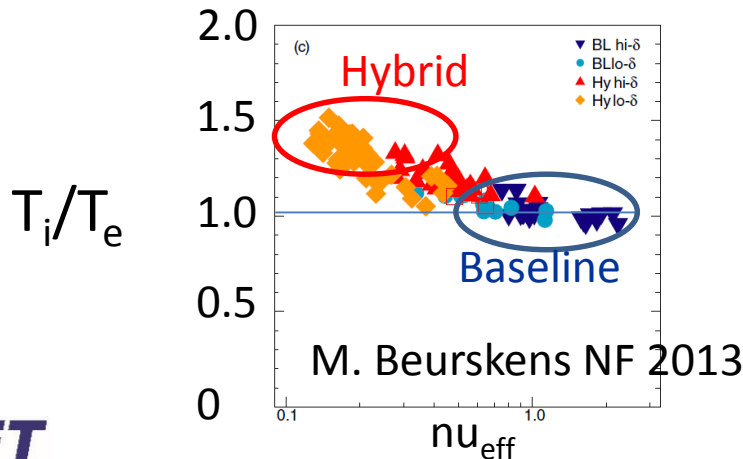


2016 JET-ILW baseline discharges



1) The fusion performance achieved in 2016 (i.e. #92436) was much better than that expected based on previous experiments with the same high heating power in 2014 (i.e. #87412). Why?

2) Previously, high T_i/T_e was observed only in hybrid and advanced discharges where n_e is low. How could 2016 baseline discharges achieve $T_i > T_e$, despite the high n_e (i.e. $n_e > 7 \times 10^{19} \text{m}^{-3}$)?



3) High T_i/T_e was not observed in the previous discharges with the same high heating power (i.e. #87412). How was it possible only in 2016?



1.Database

2.Setting for statistical TRANSP analysis

3.Answers to the three key questions

4.Summary



- ❖ 115 H-mode discharges from the 2016 baseline scenario development were selected.
- ❖ http://users.euro-fusion.org/tfwiki/images/1/1b/M15-01_GoodPulsesList_4wiki.xls
 - Pulse number : 89062 - 92442
 - $I_p = 2.16 - 3.47$ [MA]
 - $B_t = 2.35 - 3.03$ [T]
 - $P_{NBI} = 7.22 - 27.79$ [MW]
 - $P_{ICRF} = 0.8 - 6.34$ [MW]
 - $n_{e0} > 7e19$ [m⁻³]
 - $q_{95} = 2.72 - 3.75$
 - **Deuterium Gas puffing = 0 - 9e22 [sec⁻¹]**

Setting for statistical TRANSP analysis



- **Measured T_i is not available** in all discharges due to the difficulty of the CX data analysis in ITER-Like Wall i.e. No Carbon!
- Alternatively, statistical analysis of interpretive TRANSP runs were performed.
 - ✓ **$T_i = T_e$ was assumed in TRANSP runs of all 115 discharges**
 - ✓ **For subset 11 discharges, where CX measurement is available, measured T_i was used for TRANSP runs**
- Except the above mentioned, an identical setting was used for all TRANSP analysis
 - ✓ Fitted HRTS T_e and n_e
 - ✓ Z_{eff} from Visible Bremsstrahlung assuming uniform profile
 - ✓ 100% Be or 100% Ni impurity assumption (used for error bars).
 - ✓ Total bulk Radiation from Bolometry assuming uniform radiation profile
 - ✓ NUBEAM (30000 Monte Carlo ptls)
 - ✓ TORIC (dipole phasing with $N_{\text{phi}}=27$, H minority, 3% concentration)
 - ✓ q profile from EFIT
 - ✓ Boundary equilibrium from EFIT
 - ✓ Internal equilibrium calculated by TEQ

Key questions on 2016 baseline discharges

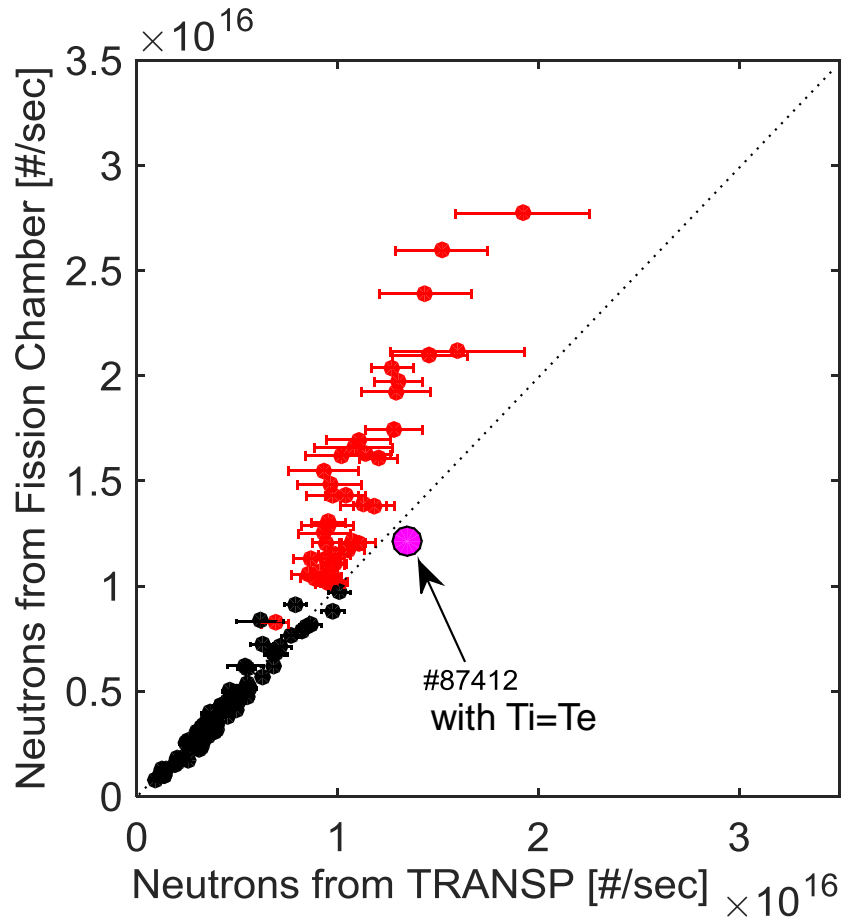


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Statistical Investigation on $T_i > T_e$

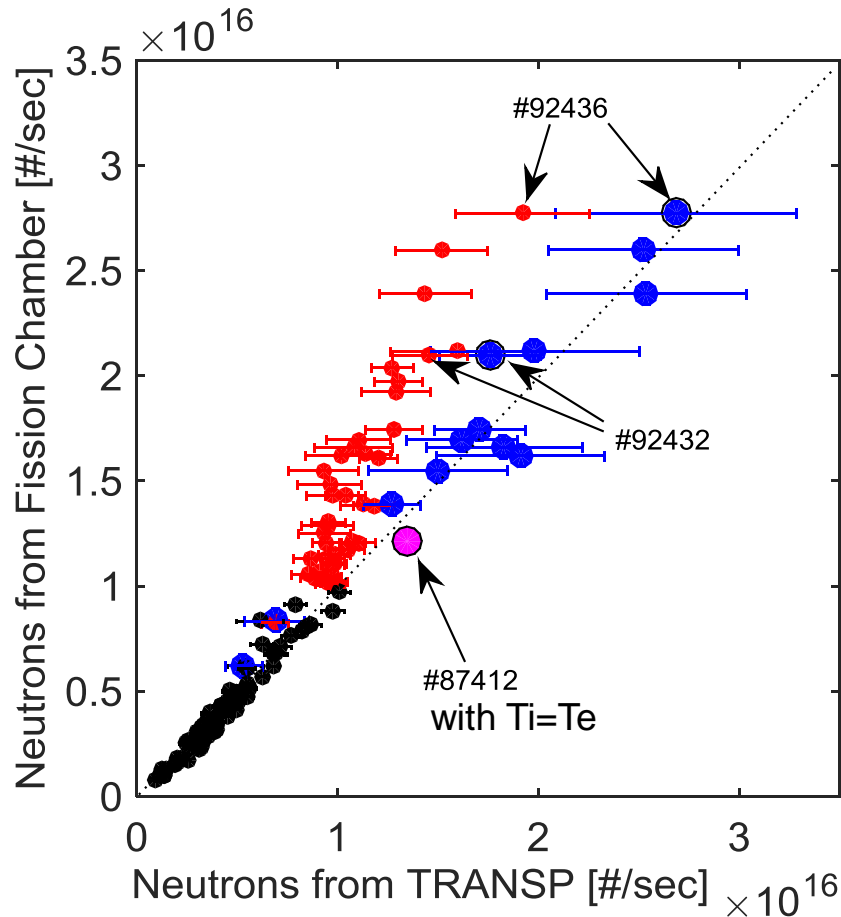


High neutrons with $T_i = T_e$ in TRANSP
Low neutrons with $T_i = T_e$ in TRANSP

- TRANSP runs with $T_i = T_e$ assumption underestimates the total neutrons at high heating power (>25MW).

The error bars are the calculated neutrons with different impurity assumptions i.e. 100% Beryllium (left bar) or 100% Nickel (right bar)

Statistical Investigation on $T_i > T_e$

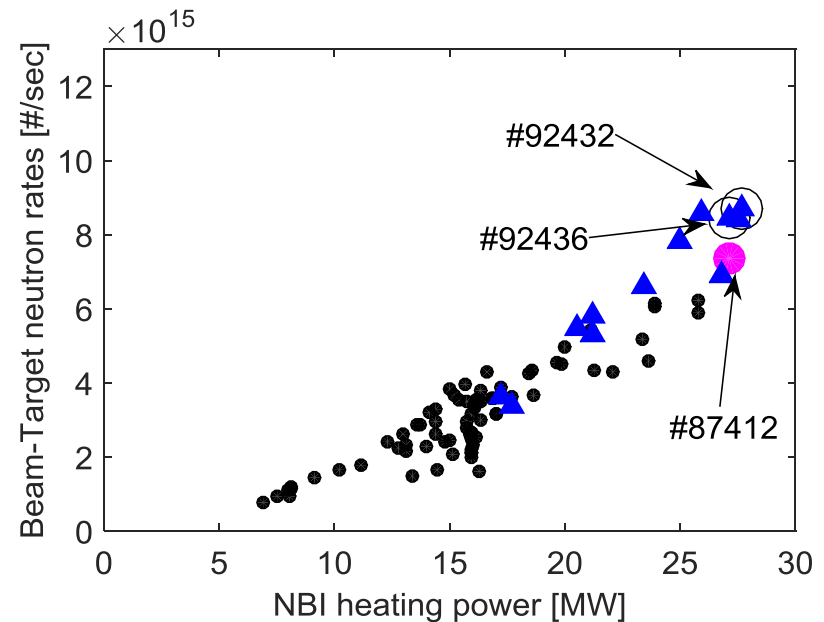
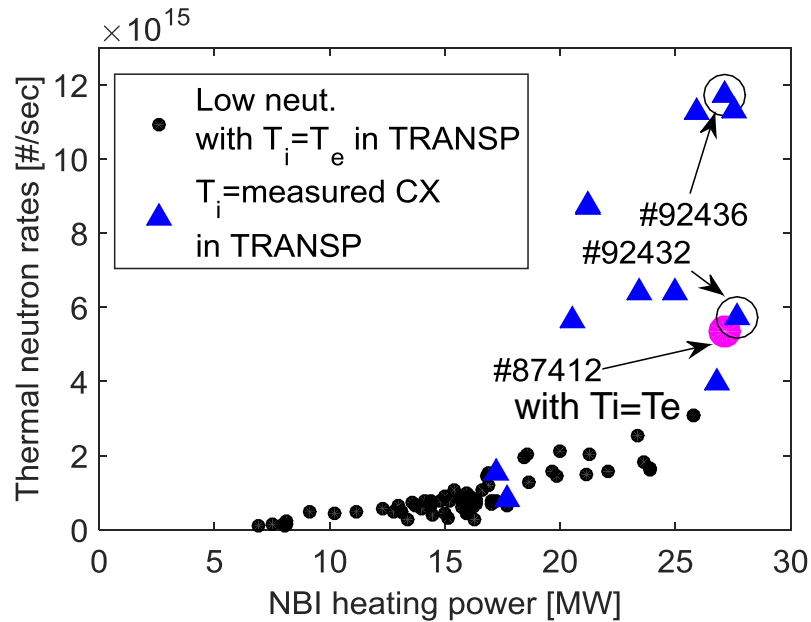


High neutrons with $T_i=T_e$ in TRANSP Low neutrons with $T_i=T_e$ in TRANSP $T_i=CX$ measurement in TRANSP

- TRANSP runs with $T_i=T_e$ assumption underestimates the total neutrons at high heating power (>25MW).
- TRANSP neutron predictions consistent with neutron measurements when measured $T_i (>T_e)$ were used in the subset discharges .

The error bars are the calculated neutrons with different impurity assumptions i.e. 100% Beryllium (left bar) or 100% Nickel (right bar)

Neutron analysis



Increase in thermal neutron rate is the main contribution for the high fusion performance, rather than beam-target neutrons.

High T_i , exceeding T_e , is the key factor.

Key questions on 2016 baseline discharges



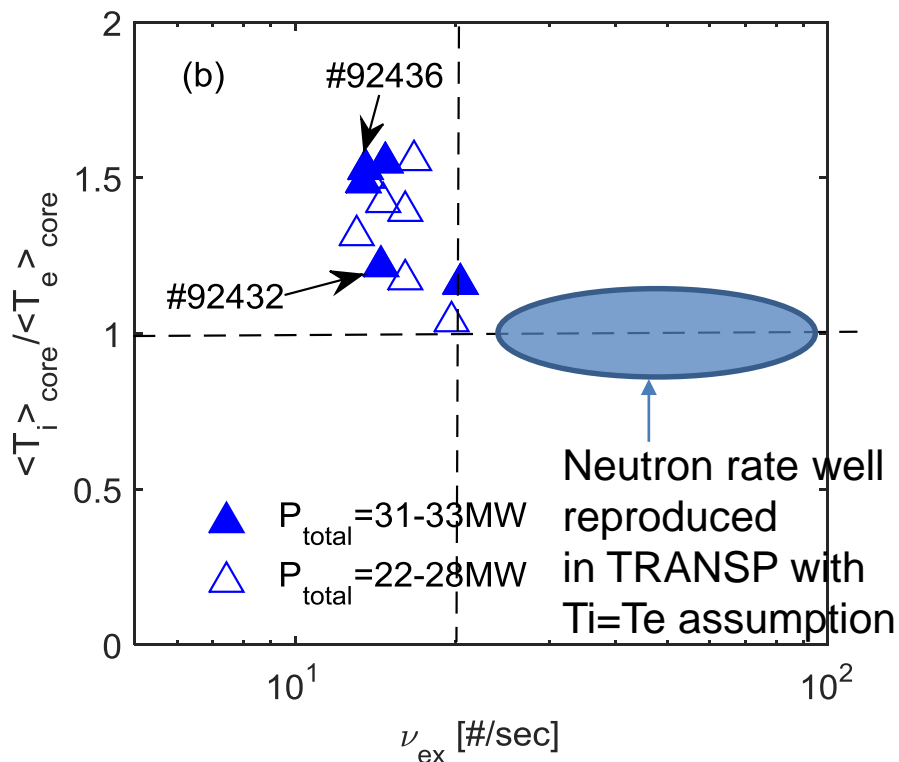
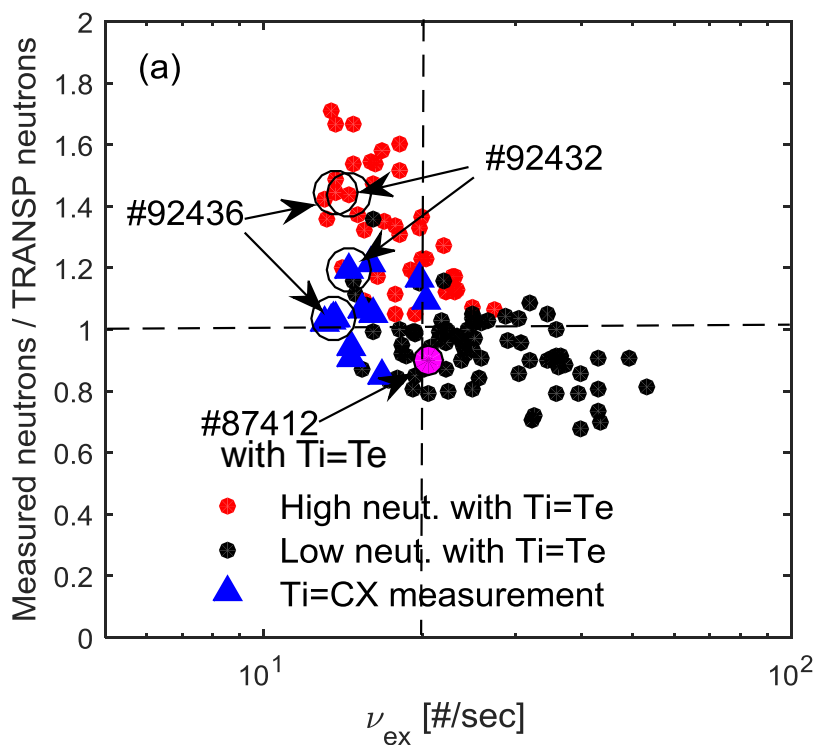
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Collisionality

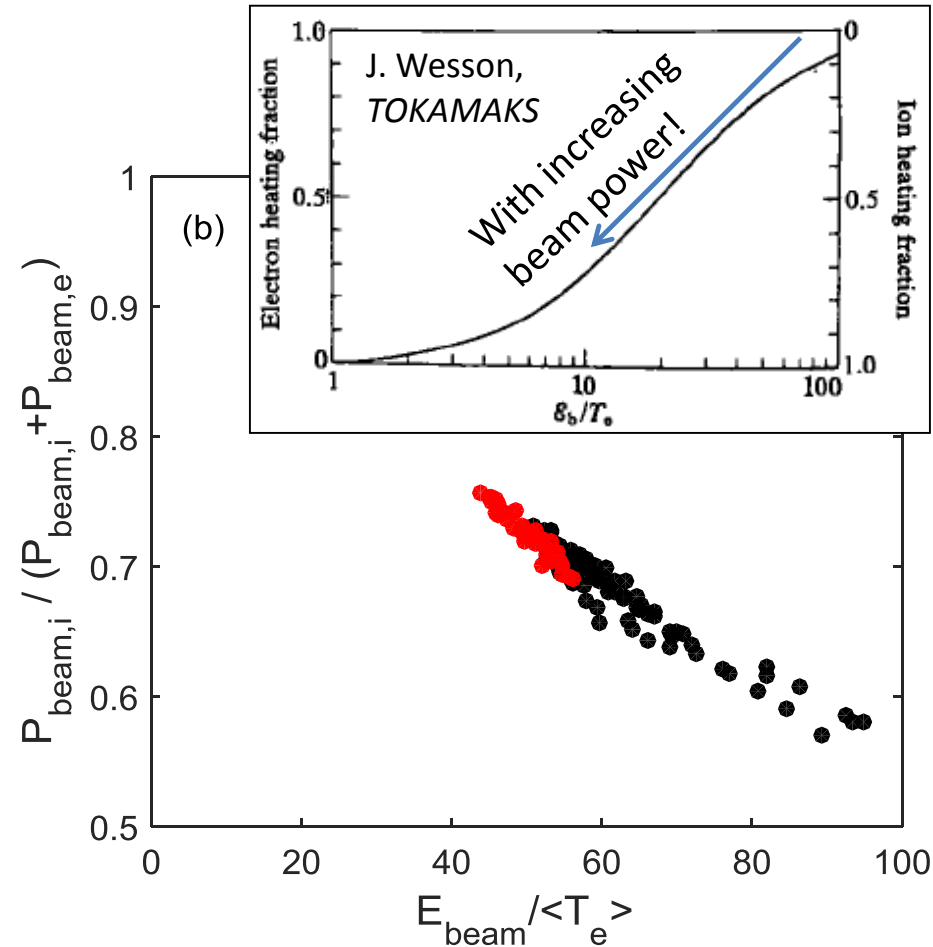
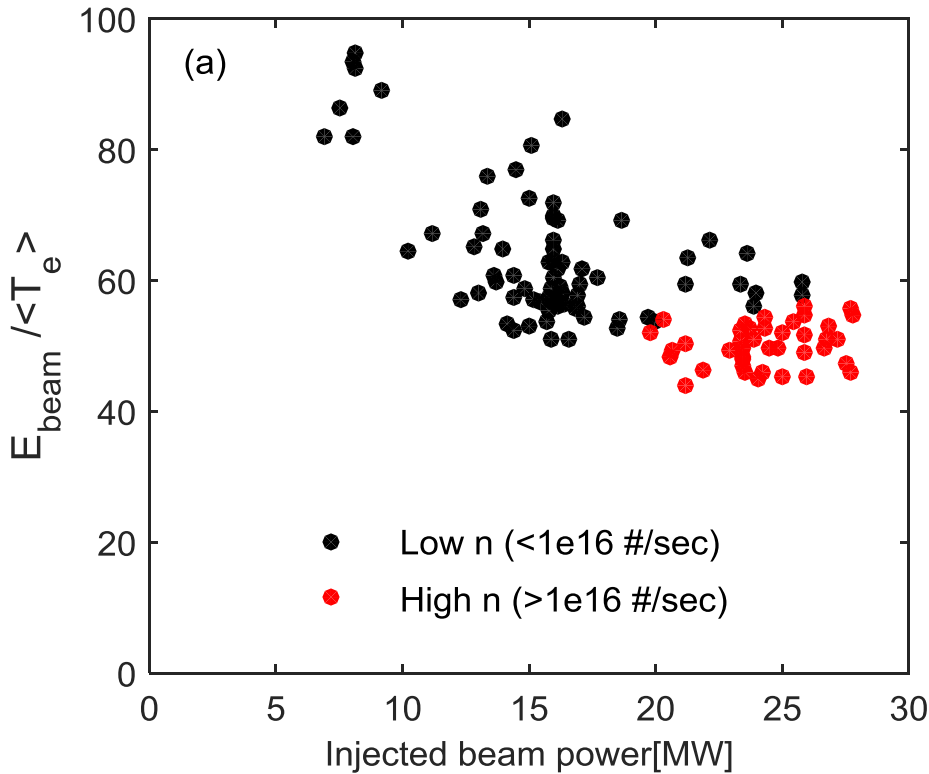


- The neutron under-estimation with $T_i=T_e$ in TRANSP is more significant at low collisionality regime i.e. $T_i > T_e$ at low collisionality.

$$\nu_{ex} \equiv 0.32 \times 10^{-14} \frac{m_e \langle n_e [m^{-3}] \rangle}{m_i \langle T_e [keV] \rangle^{3/2}}$$

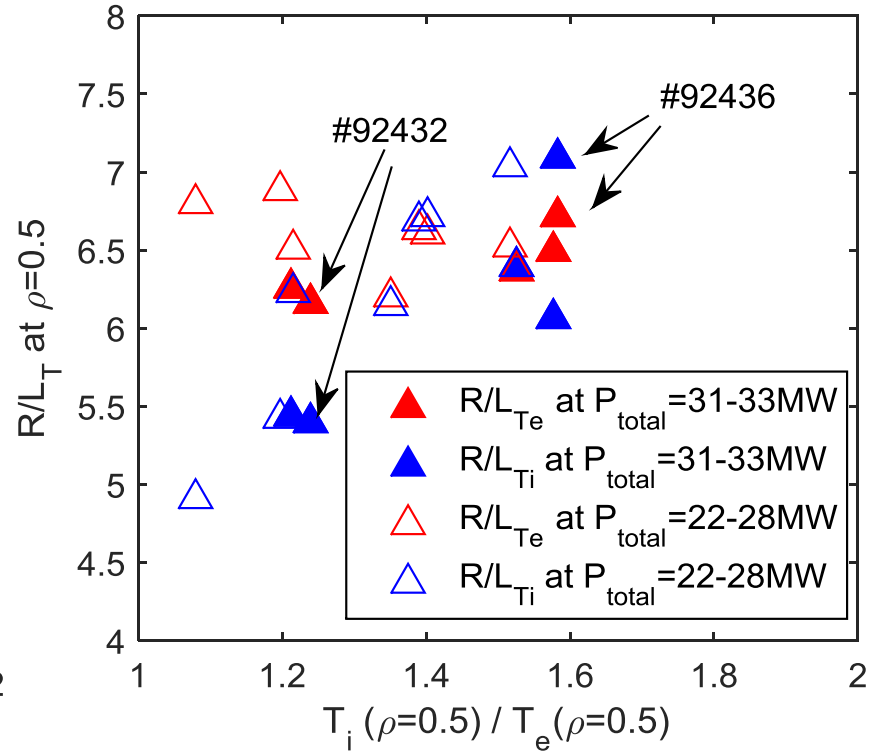
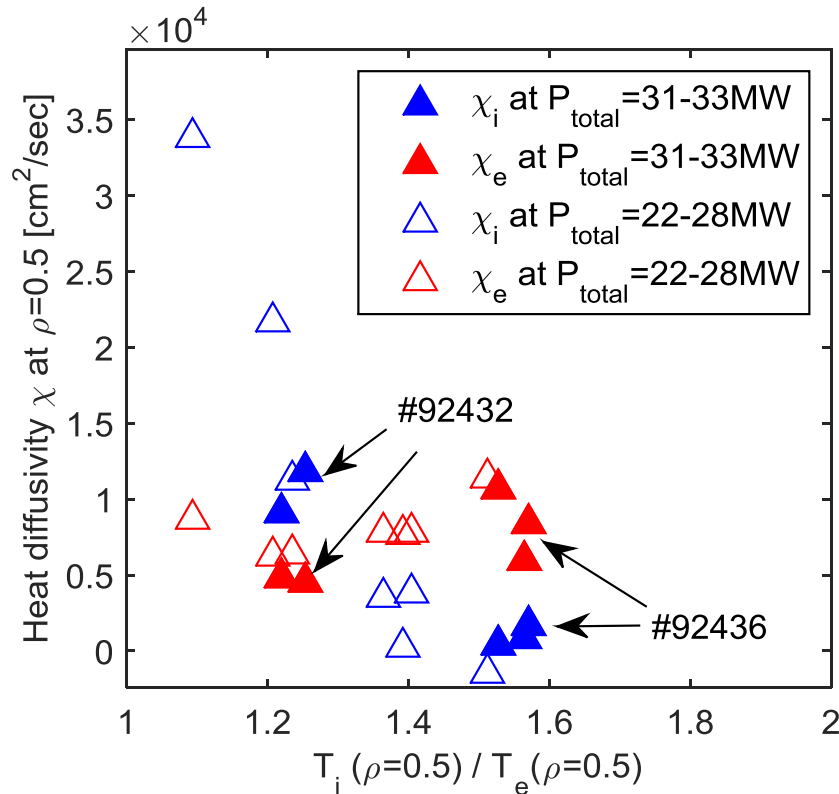
- High heating \rightarrow Increase in $T_e \rightarrow$ sufficient decrease in collisionality (despite high n_e) \rightarrow Low equilibration power \rightarrow decoupling T_i from T_e .

Heating power analysis



High beam power increases T_e , thereby decreasing $\epsilon_{\text{beam}} / T_e$.
 → ion heating fraction increases.

Transport analysis



Ion heat transport is reduced with high T_i/T_e ,
while electron heat transport isn't.

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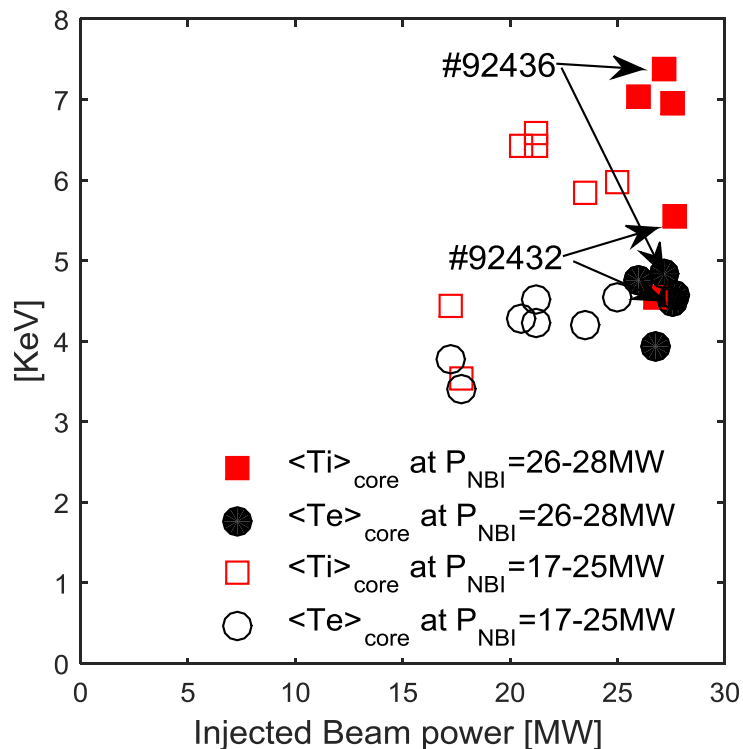
→ $P_{\text{heat}} (> 25 \text{MW})$ was high enough to decrease the collisionality despite high n_e

→ Ion heating fraction increases with heating power

→ Ion heat transport was reduced with high T_i/T_e

3) High T_i/T_e was not observed in the previous discharges with the same high heating power (i.e. #87412). How was it possible only in 2016?

Requirements for $T_i > T_e$

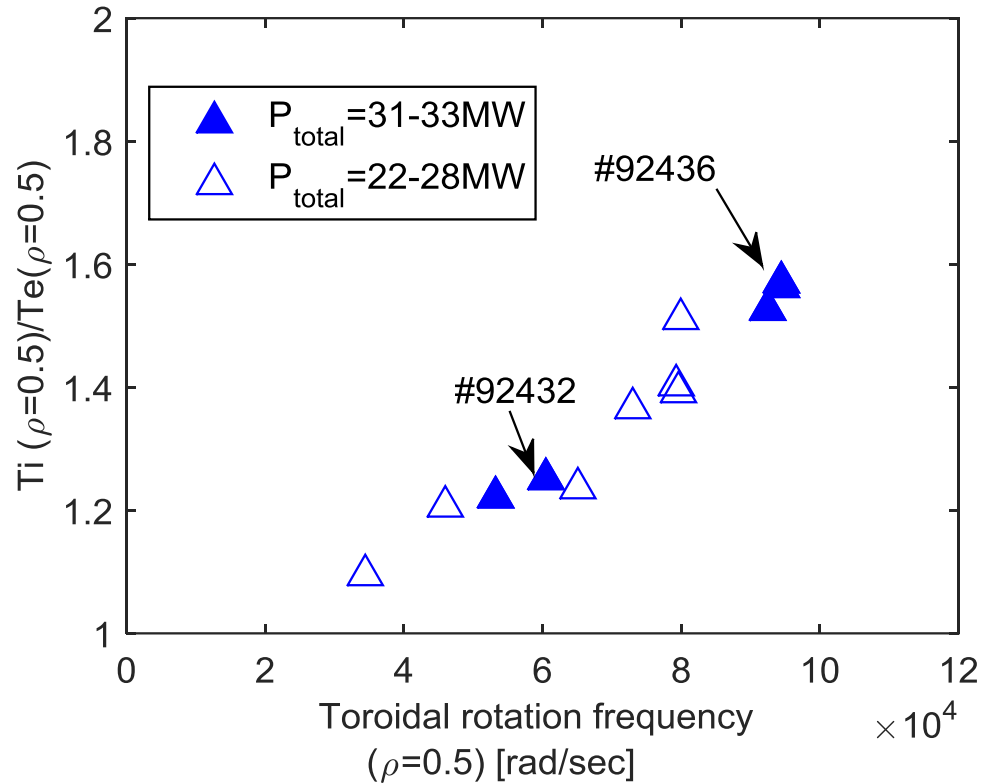


Requirements for high T_i/T_e

1. Low collisionality to decouple T_i and T_e
2. High ion heating fraction
3. Low ion heat transport

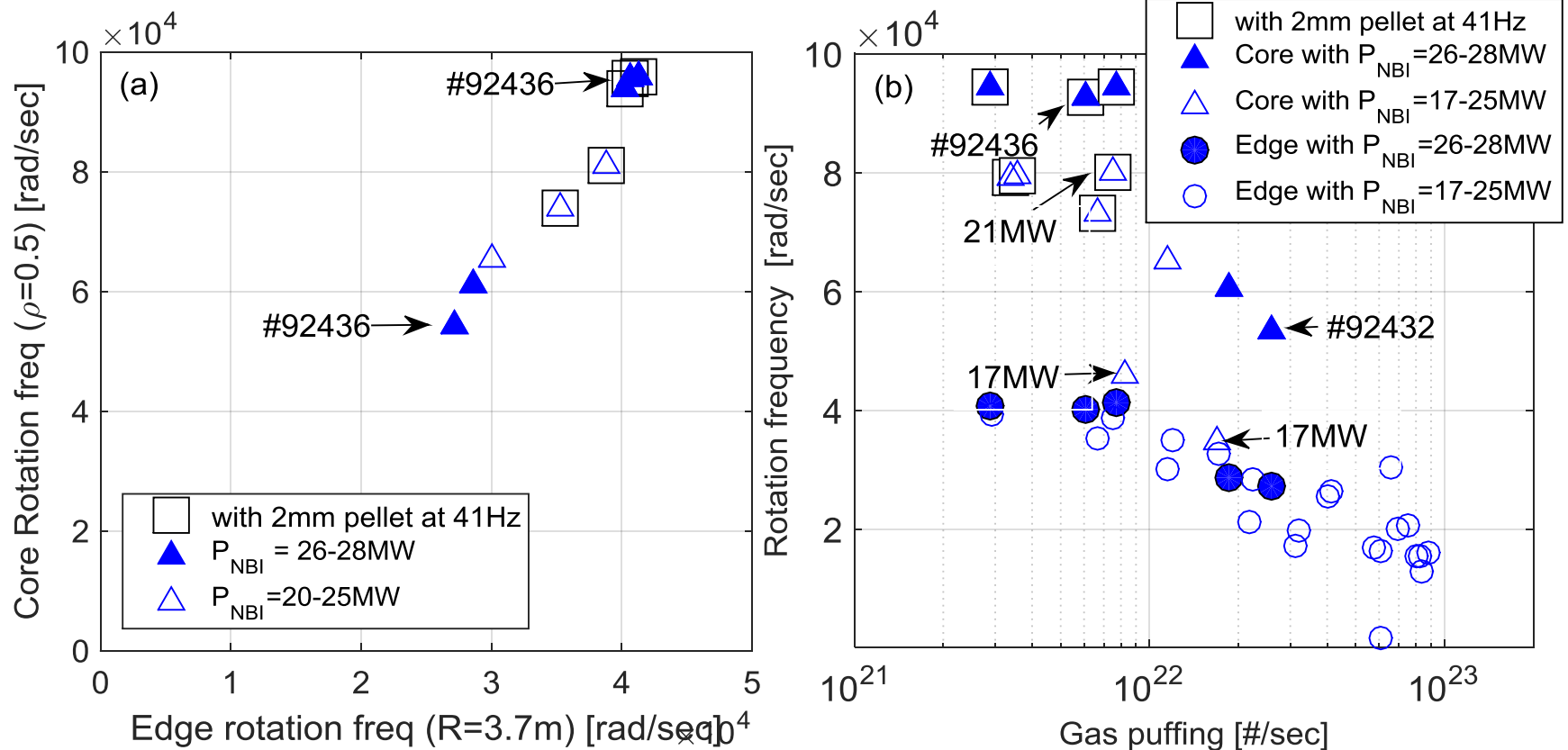
However, high beam power alone cannot explain the high T_i/T_e .

Impact of rotation



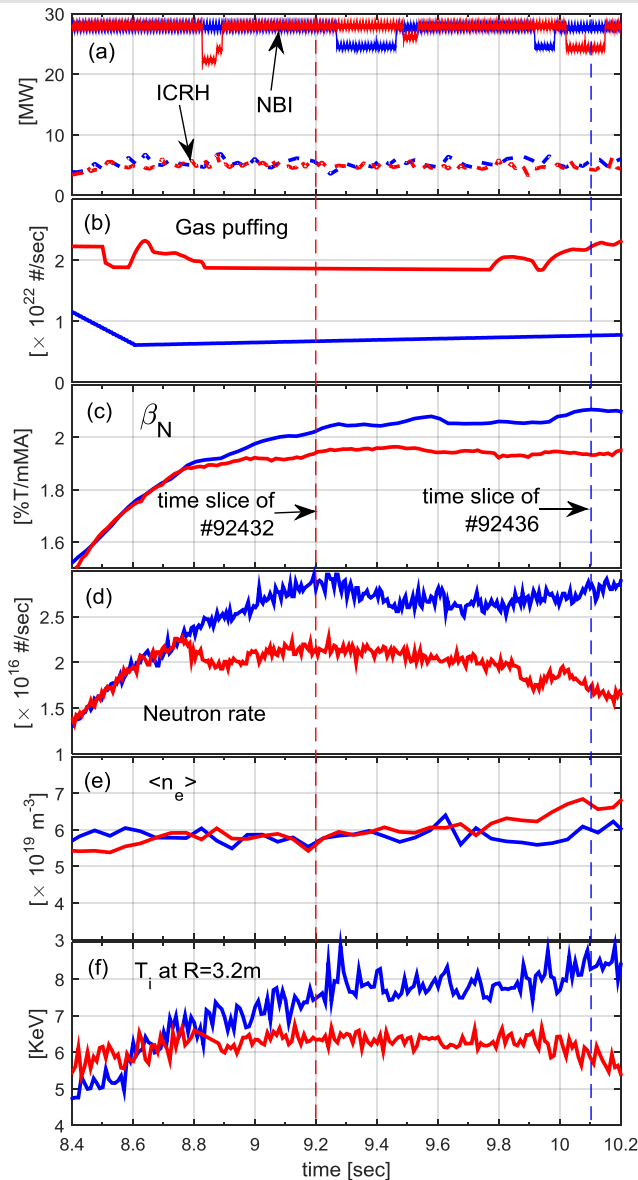
Core T_i/T_e is correlated with core rotation frequency.

Impact of gas puffing



- Core rot freq is correlated with edge rot freq, which is correlated with low gas puffing.
- Thanks to the use of ELM pacing pellets, low gas injection operation was possible, while keeping ELMs frequent enough.
- For high rot freq, high beam power is required for high momentum source, but low gas fuelling should be also important as neutrals at the edge may be a strong momentum sink.

#92436 and #92432

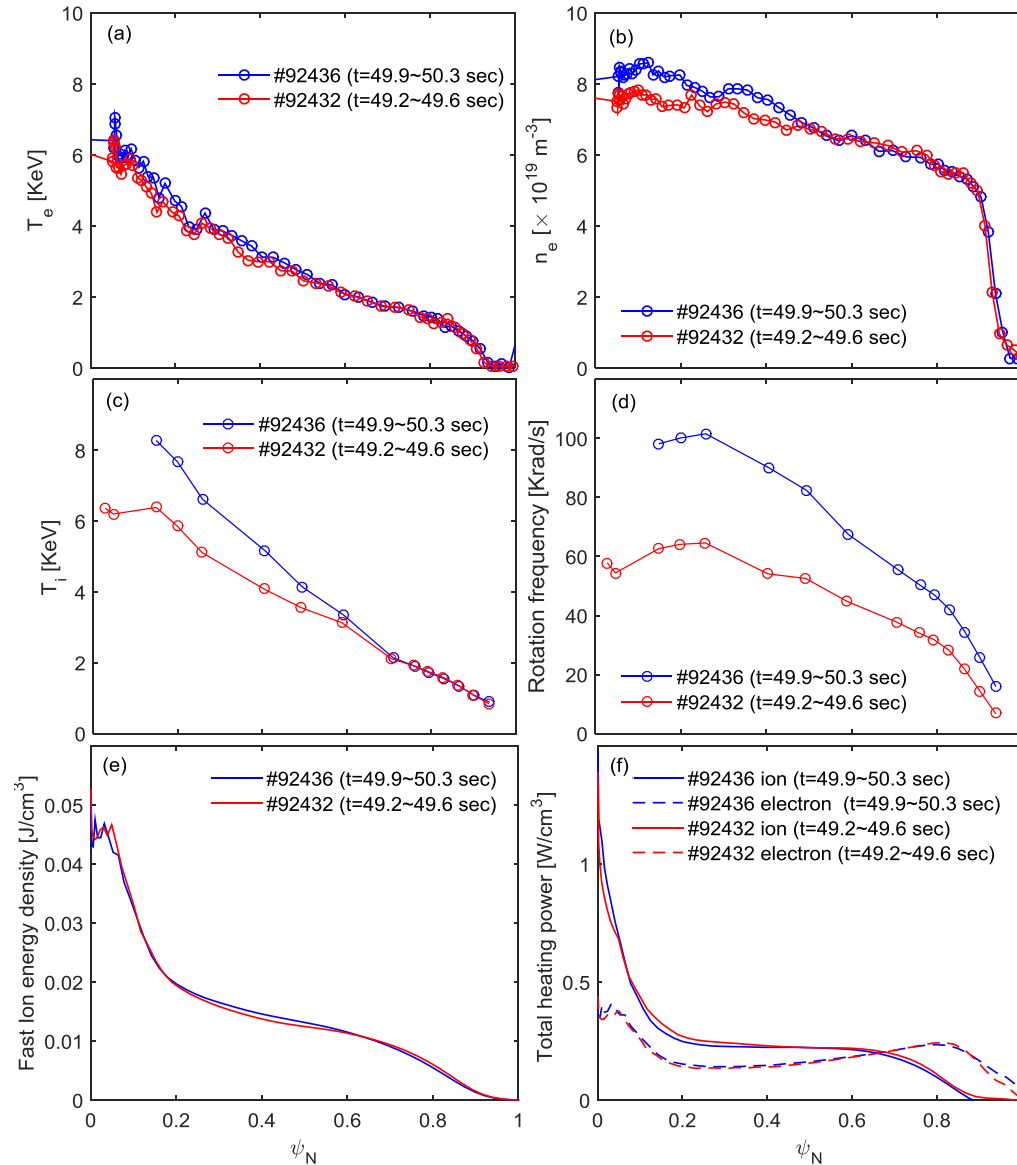


— #92436 — #92432

Identical control room parameters in the two discharges, except gas fuelling

	92436	92432
I_p	3MA	3MA
B_t	2.8T	2.8T
P_{NBI}	27.5MW	27.5MW
P_{ICRH}	5MW	5MW
Gas	7e21 #/sec	2e22 #/sec
H98	1.1	1.0
Neutron Yield	2.8e16 #/sec	2.1e16 #/sec

#92436 and #92432



Similar T_e and n_e profiles

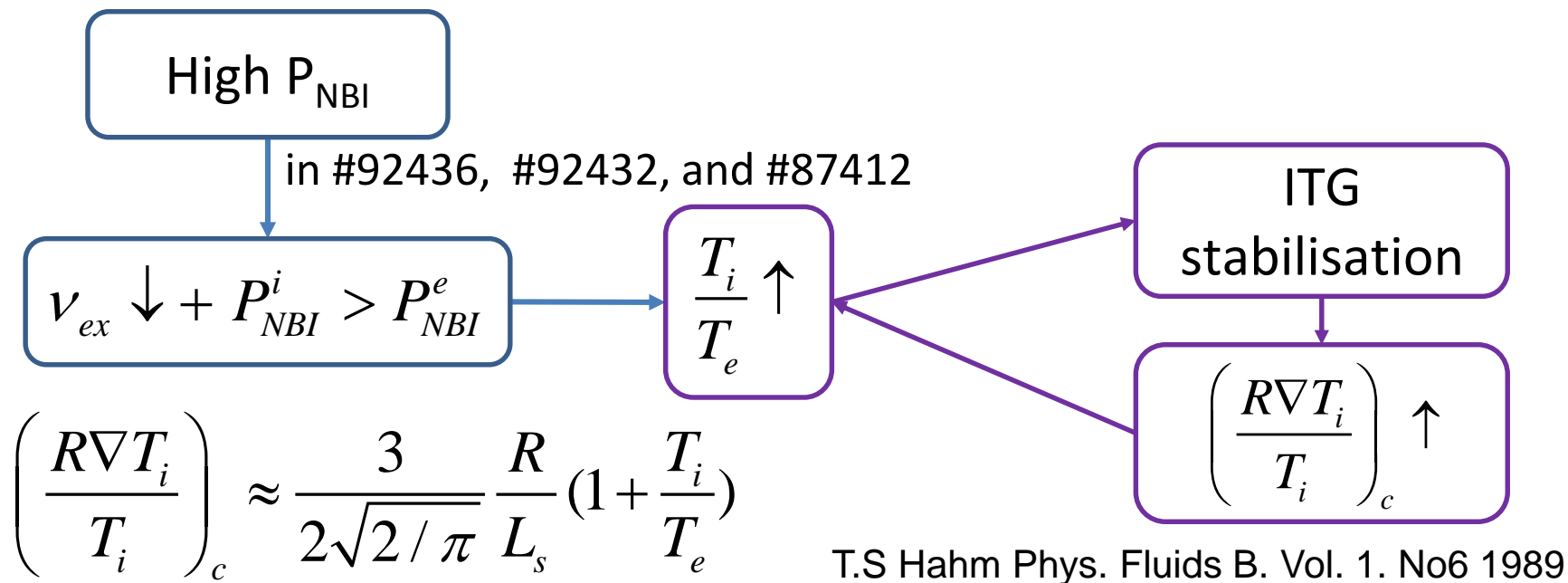
Similar fast ion distribution

Similar heating profiles

Rotation is clearly higher in #92436 (low gas) than in #92432 (high gas)

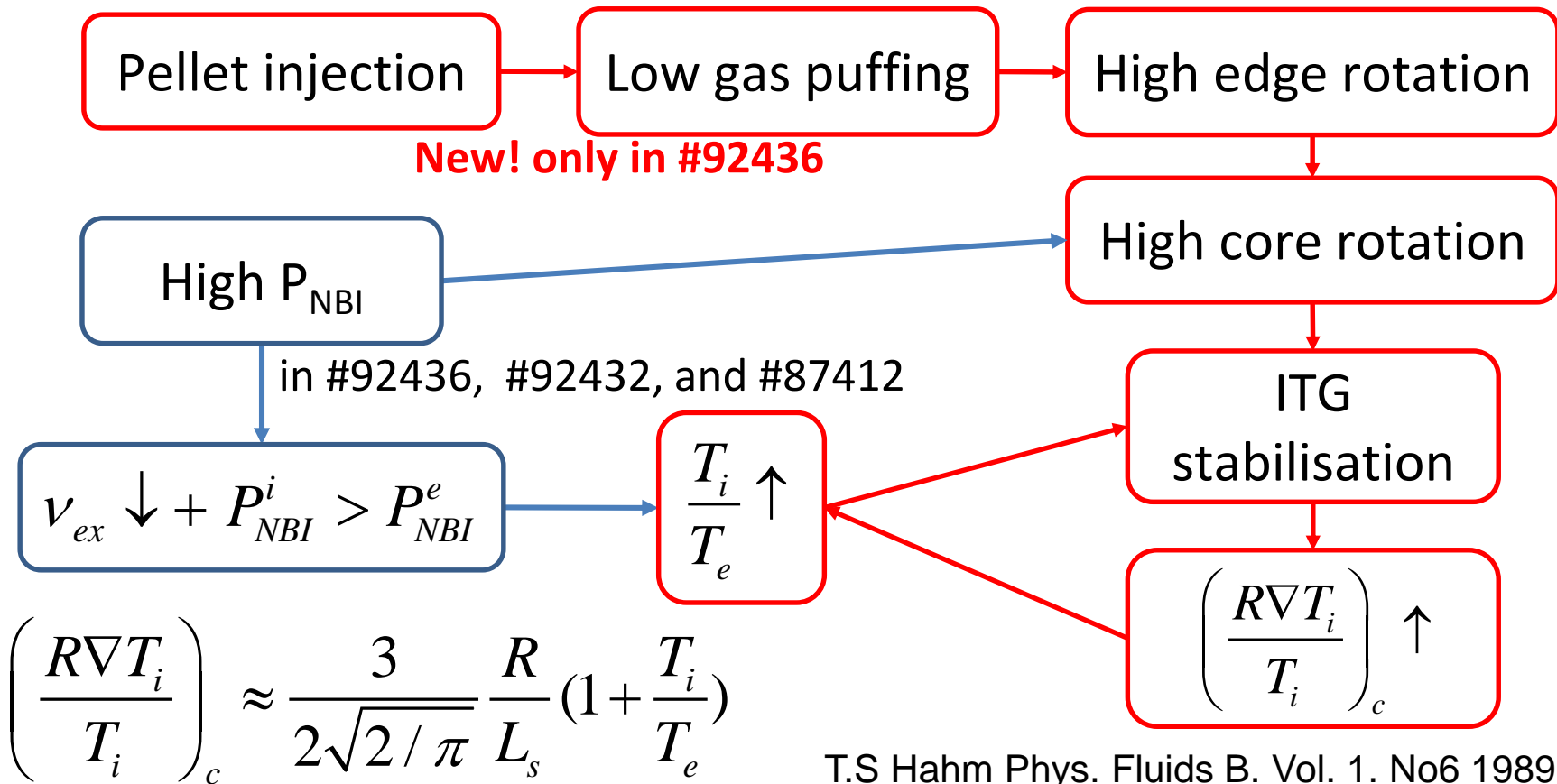
Higher core T_i in #92436

Possible explanation on high T_i/T_e



- High P_{NBI} , reducing collisionality and increasing ion heating ratio, enabled $T_i > T_e$.
- High T_i/T_e is also correlated with low ion heat transport i.e. positive feedback between high T_i/T_e and ITG stabilisation

Possible explanation on high T_i/T_e



- Low gas puffing increases rotation freq, helping further ITG stabilisation.
- Use of low gas puffing was possible by pellet injections, which were the only main difference in #92436, compared to #92432 and #87412

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→ $P_{heat} (> 25 MW)$ was high enough to decrease the collisionality despite high n_e

→ Ion heating fraction increases with heating power

→ Ion heat transport was reduced with high T_i/T_e

3) High T_i/T_e was not observed in the previous discharges with the same high heating power (i.e. #87412). How was it possible only in 2016?

→ High T_i/T_e is correlated with high rotation frequency.

→ Rotation frequency increases with low gas puffing.

→ Low gas puffing was only possible in 2016 baseline discharges, thank to the pellet injections.

Summary



- 2016 baseline discharges with high beam power (max. 28MW) achieved a very good fusion performance. This comes from core confinement improvement (not only from the pedestal).
- High T_i , exceeding T_e , was observed in baseline discharges despite the high n_e . This enabled the high neutron yield.
- High T_i/T_e was possible because of
 1. Low collisionality
 2. High fraction of beam heating to ions
 3. Reduced ion transport, which should be due to the positive feedback between high T_i/T_e and ITG stabilisation.
- **High T_i/T_e is correlated with high rotation freq**, implying ExB flow shear may improve the positive feedback.
- **High rotation is not only correlated with high beam power, but also with low gas puffing, which was possible by pellet injections in 2016.** Neutrals at the edge could be a momentum sink.
- Further details available in *Hyun-Tae Kim et al, NF 58 (2018) 036020*