

First operation of the Wendelstein 7-X stellarator and expectations for the future

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on behalf of the Wendelstein 7-X Team

HELMHOLTZ
SPITZENFORSCHUNG FÜR
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The logo for EUROfusion, featuring a stylized blue circular design of concentric arcs.
EUROfusion



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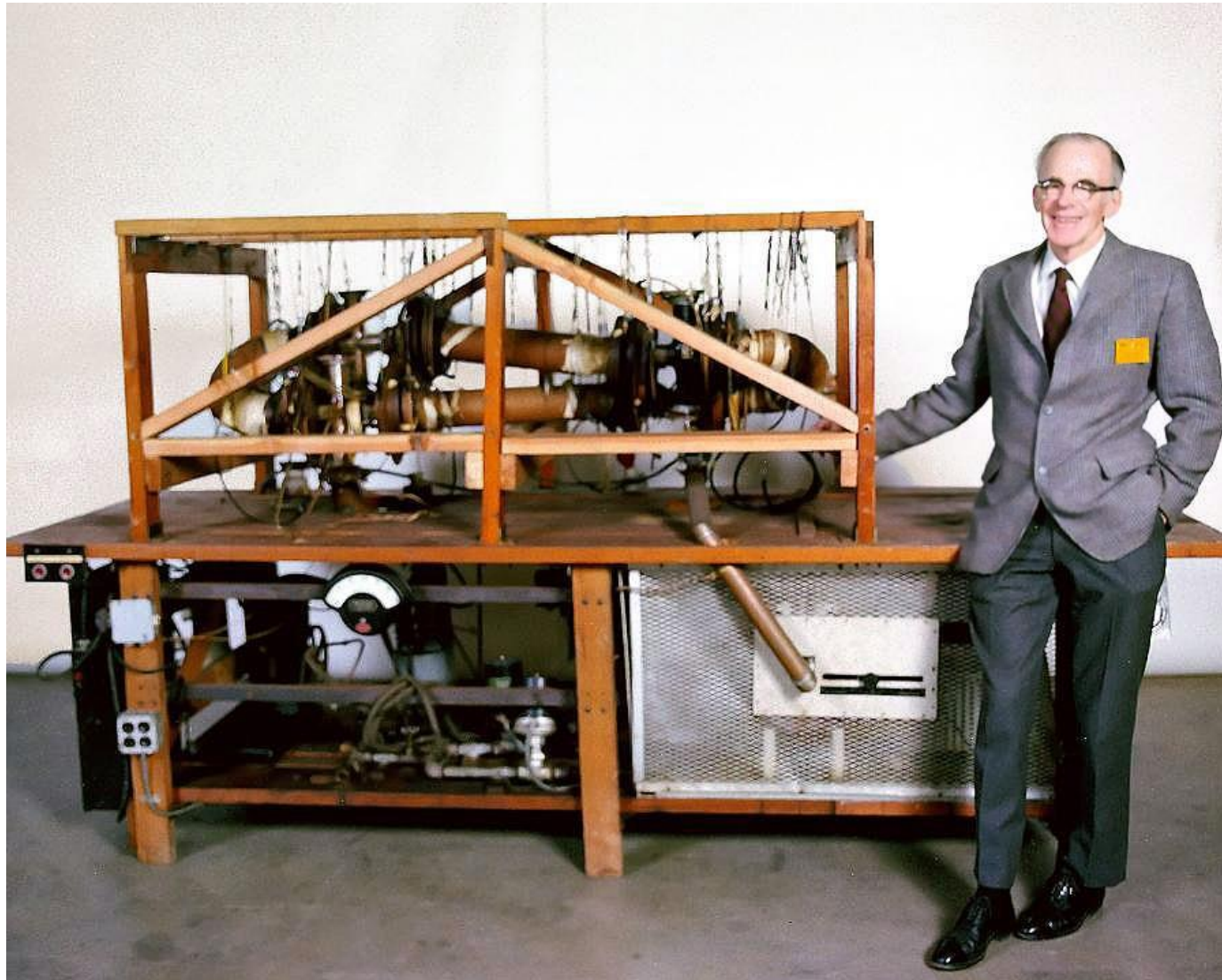
Content of the talk

One-team approach for operation:

- The W7-X Team includes researchers and engineers from IPP, Euratom, US (DoE), and Japan.
- It will be published in the Nuclear Fusion paper of the IEAE FEC 2018.

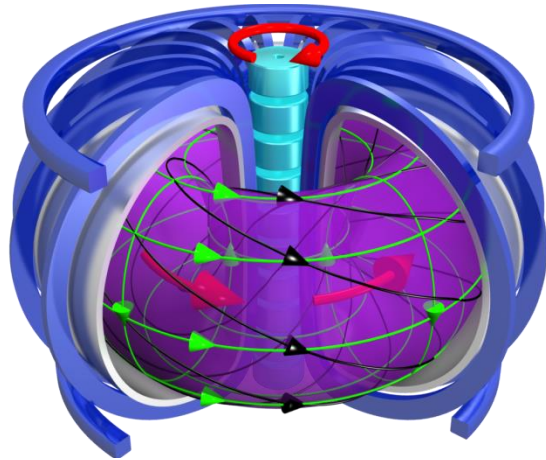
Content of the talk

1. Why stellarators?
2. Technologies of W7-X
3. Performance
4. Conclusions and the future



- 1951 invented by Lyman Spitzer jr. in Princeton in a classified report.
- Project Matterhorn
- First stellarator operated in early 1953, as figure-8 or racetrack.
- This picture in 1983, just before donated to the Smithsonian.
- Plasma confinement was rather bad and PPPL “switched” to tokamaks.

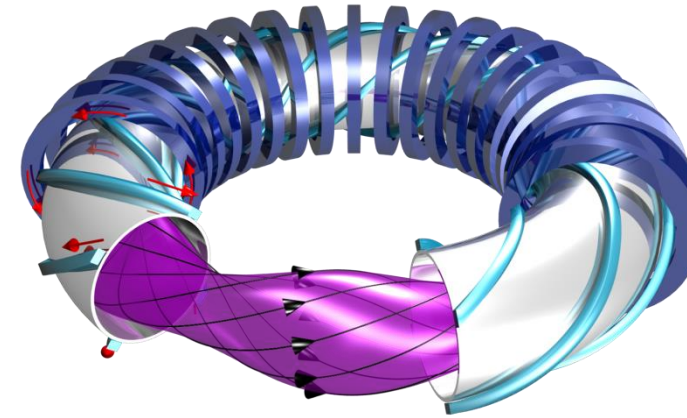
Tokamak



currents in coils and plasma

- + good heat isolation**
- + highly symmetric**
- pulsed operation**
- free energy can drive instabilities**

Stellarator

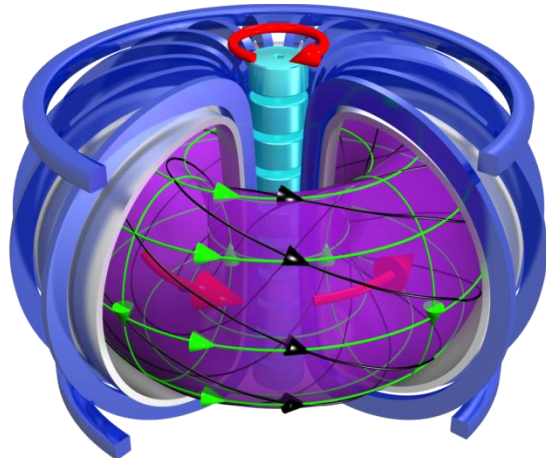


current in coils only

- bad heat isolation**
- not obviously symmetric**
- + steady state operation**
- + no current-driven instabilities**

Improved Magnetic confinement schemes

Tokamak



currents in coils and plasma

+ good heat isolation

+ highly symmetric

○ **steady state operation with current drive**

○ **active control of instabilities**

optimized Stellarator



current in coils only

○ **good heat isolation**

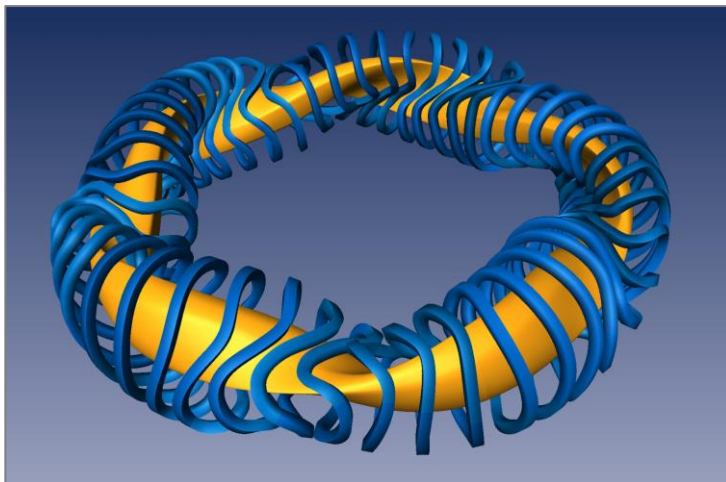
○ **quasi-symmetric**

+ steady state operation

+ no current-driven instabilities

seven optimisation criteria:

1. high quality of vacuum magnetic surfaces
2. good finite equilibrium properties @ $\langle \beta \rangle = 5\%$
3. good MHD stability properties @ $\langle \beta \rangle = 5\%$
4. reduced neoclassical transport in $1/\nu$ -regime
5. small bootstrap current in $Imfp$ -regime
6. good collisionless fast particle confinement
7. good modular coil feasibility



J. Nührenberg
et al.

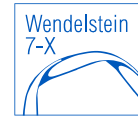
Several 3d computer codes

- vacuum field and coils
- MHD equilibrium/stability
- neoclassical transport
- Monte Carlo test particle
- edge and divertor

the mission for W7X

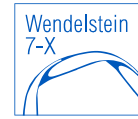
- Confirm the numerical optimisation
- Perform high power discharges, steady-state, with an energy confinement like a equivalent tokamak

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Major elements and parameters of Wendelstein 7-X



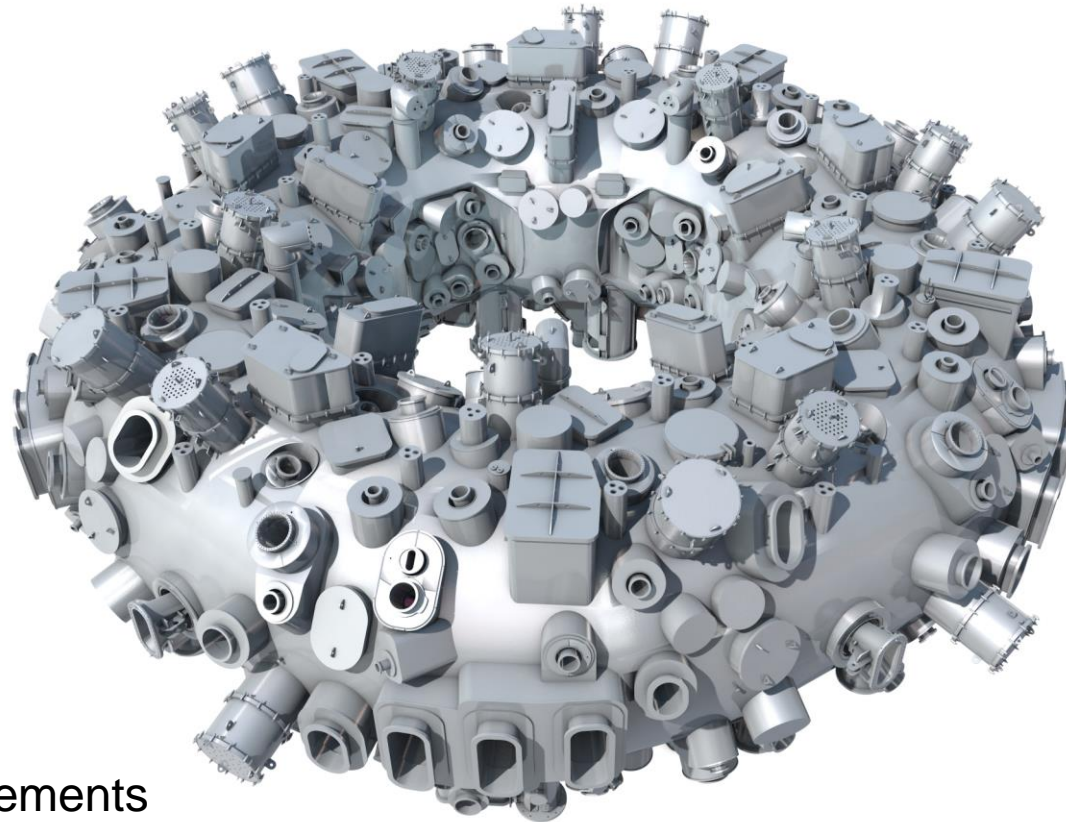
50 non-planar NbTi coils
5 types DC <18 kA

plasma 30 m³

20 planar NbTi coils
2 types DC <16 kA

plasma vessel 80 m³
265 m² in-vessel components

254 ports 120 shapes

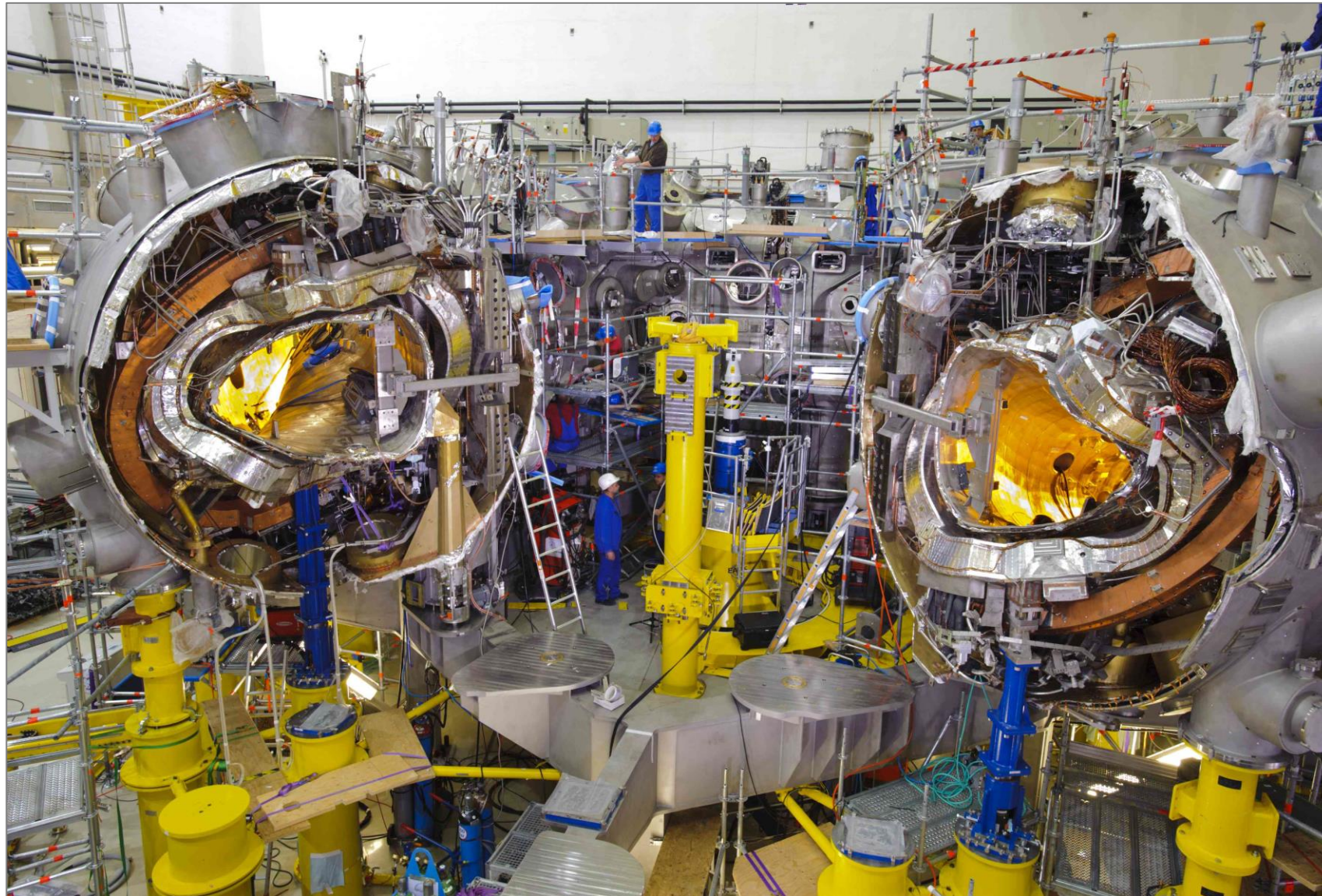


4.5 m machine height
16 m machine diameter
735 t device mass
435 t cold mass 3.4 K

113 NbTi bus bars
14 HTSC current leads
about 1000 helium pipes
10 central support ring elements

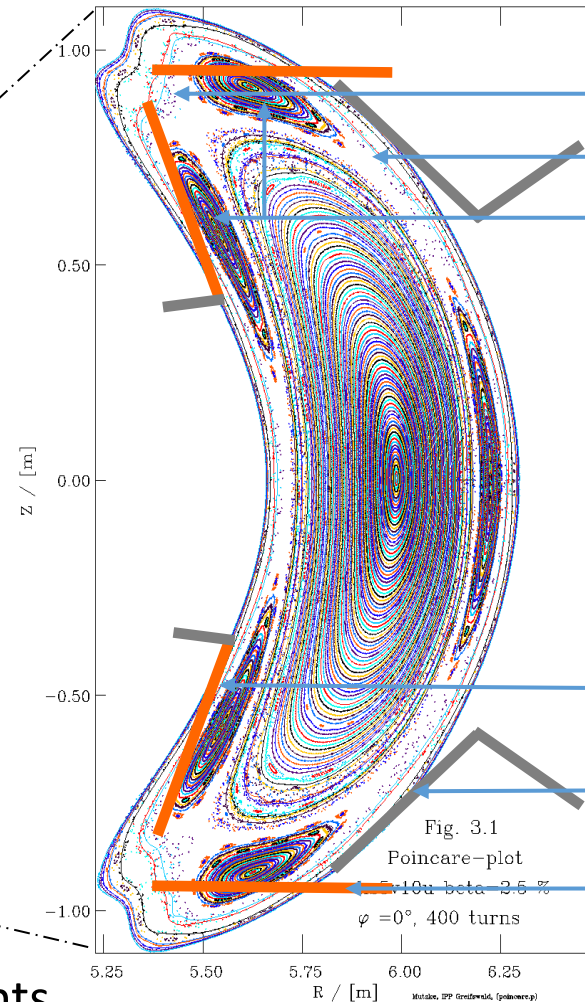
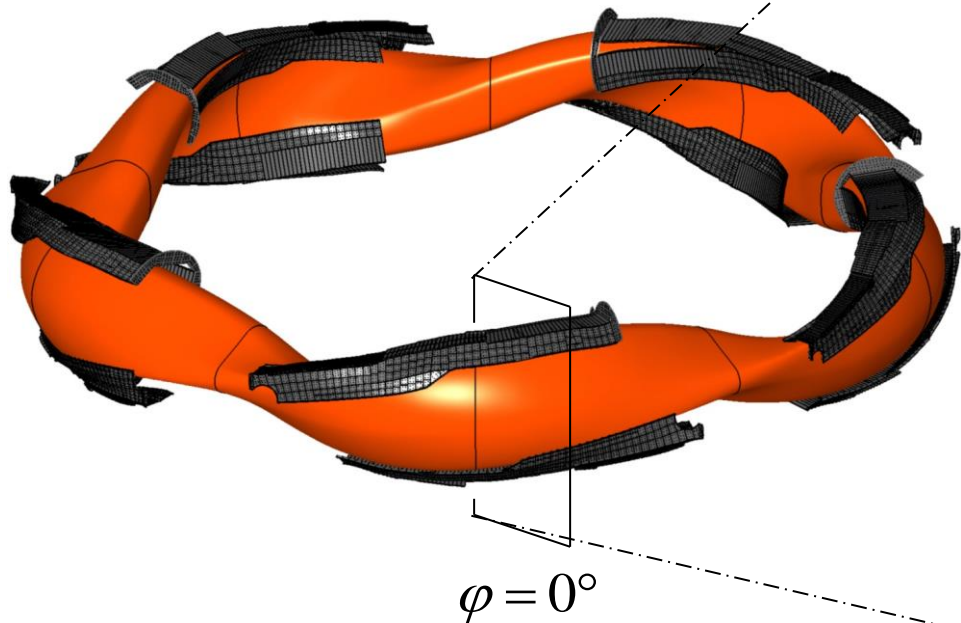
cryostat vessel 420 m³
thermal insulation

Construction of W7-X, 4/5 modules in the final position



The island divertor concept

10 island divertor modules
@ bean-shaped cross sections



X-point

ergodic region

islands

total target area 19 m²

heat flux ≤ 10 MW/m²

connection lengths ≤ 500 m

incidence angles 2-3°

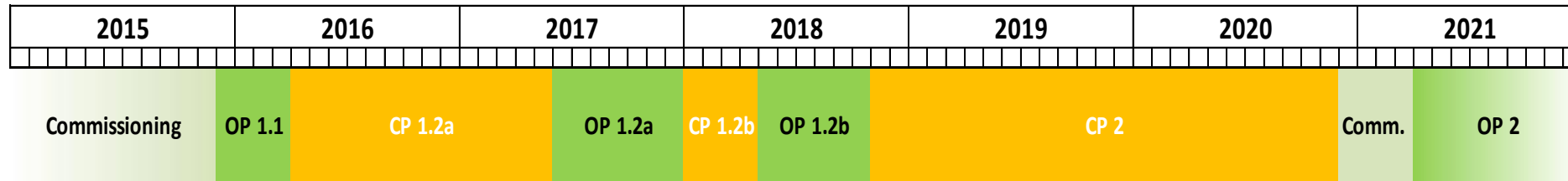
vertical target

baffle

horizontal target

initial setup with un-cooled graphite elements
future setup with water-cooled CFC elements

staged approach to the finalization of W7X



Device configuration

OP 1.1

- 5 limiters

OP 1.2a/b

- Test Divertor elements (TDU)
- Baffle elements
- Divertor closures
- Graphite wall tiles
- 2 TDU scraper elements (OP 1.2b)

OP 2

- High-Heat-Flux divertor (steady-state Water cooling)
- Port protection liners
- Cryo pumps (10 units)

Operation parameters

$$P < 5 \text{ MW}$$

$$\int P \, dt \leq 2 \text{ MJ}$$

$$\tau_{\text{pulse}} \sim 1 \text{ s}$$

$$P \leq 10 \text{ MW}$$

$$\int P \, dt \leq 80 \text{ MJ} \Rightarrow 200 \text{ MJ}$$

$$\int \tau_{\text{pulse}} \sim 10 \text{ s}$$

(... 60 s @ reduced power)

$$P_{\text{cw}} \sim 10 \text{ MW}$$

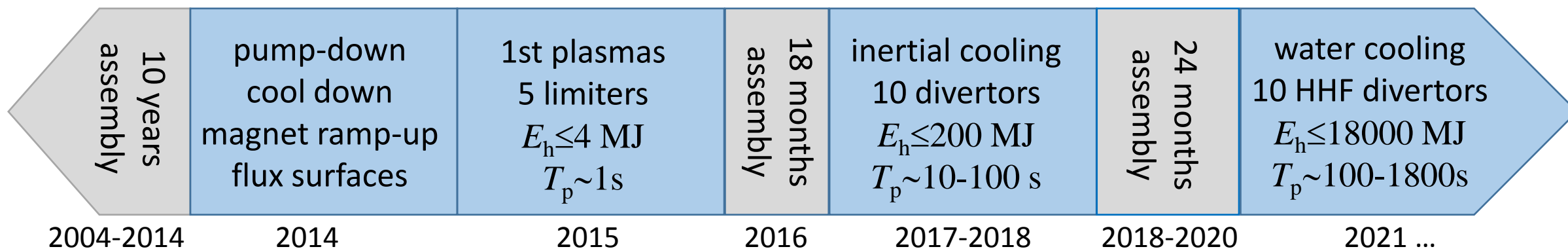
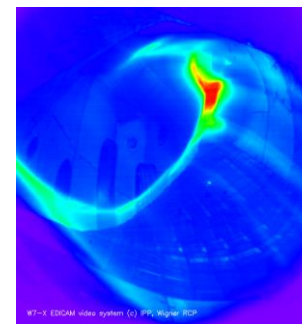
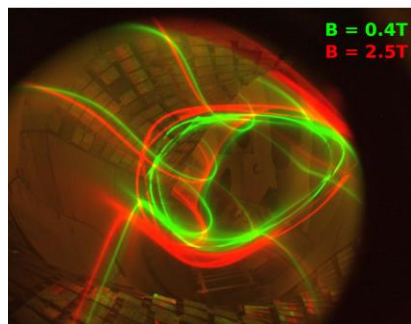
$$P_{\text{pulse}} \sim 20 \text{ MW (10 s)}$$

$$P/A \leq 10 \text{ MW/m}^2$$

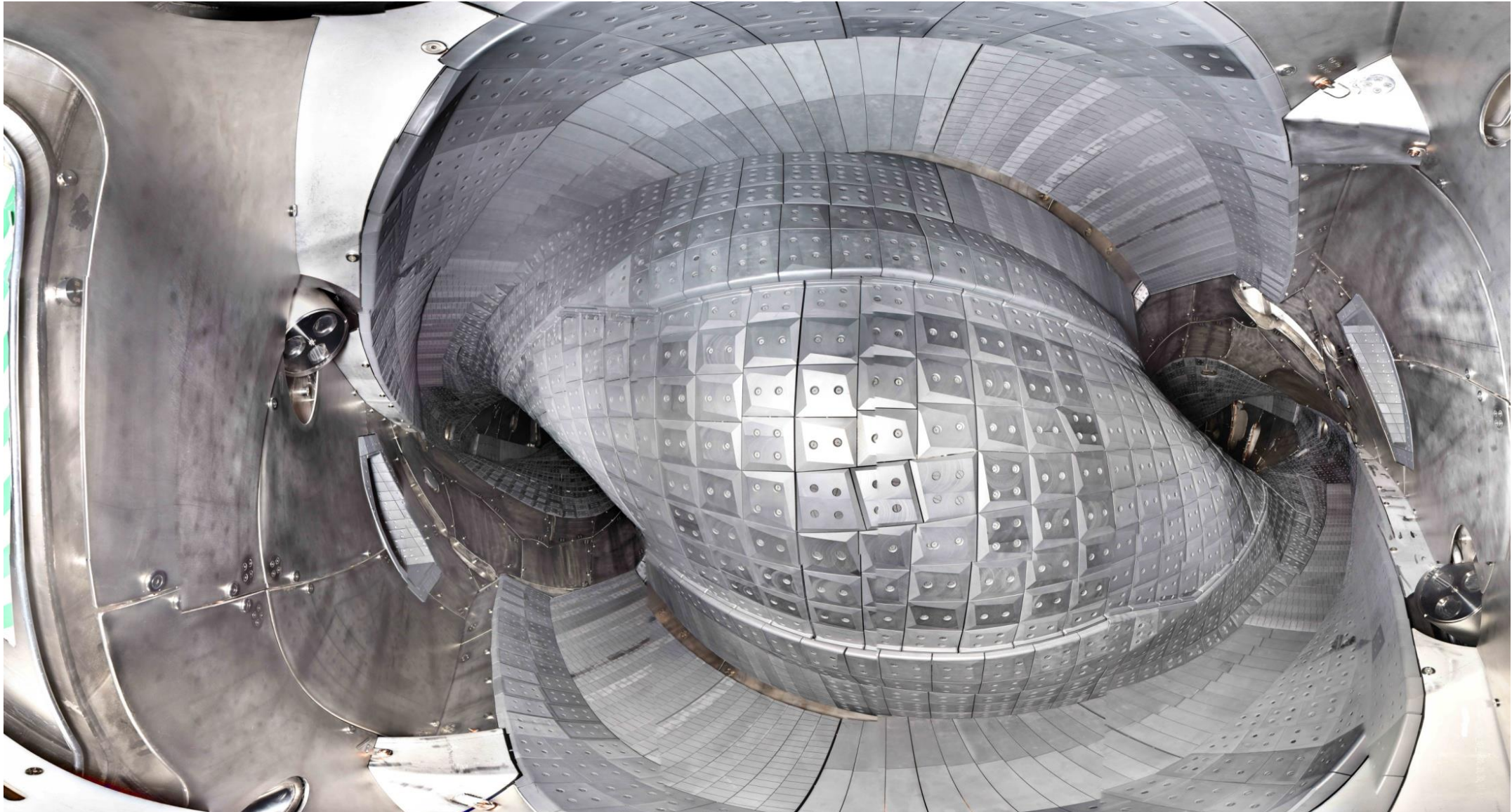
Technical limit:

30 minutes @ 10 MW

Time line of the project Wendelstein 7-X

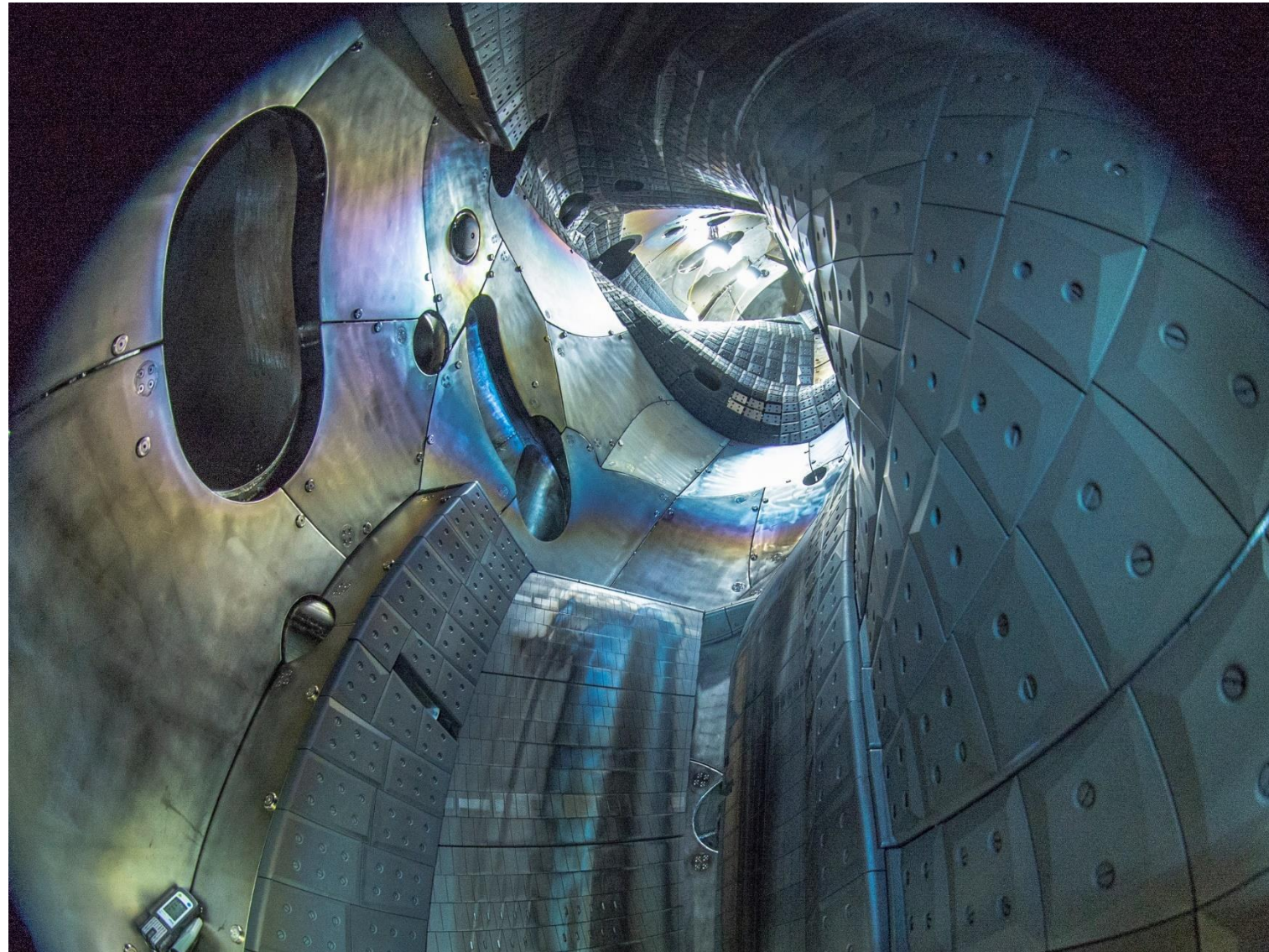


View into the plasma vessel (May 2017, module 2)

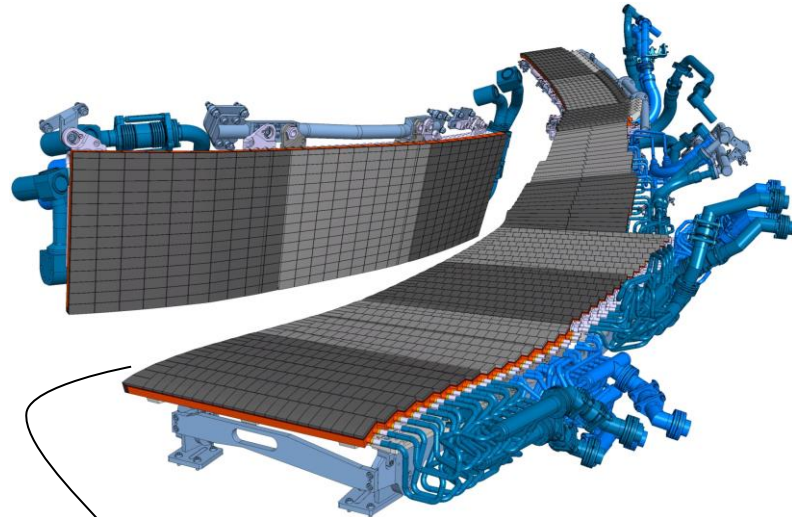


View into the plasma vessel (December 3, 2018!)

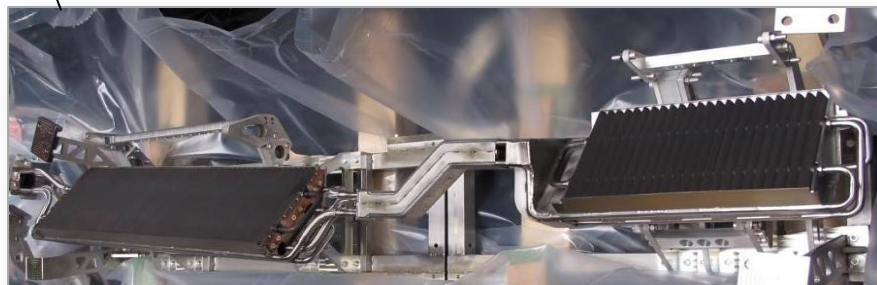
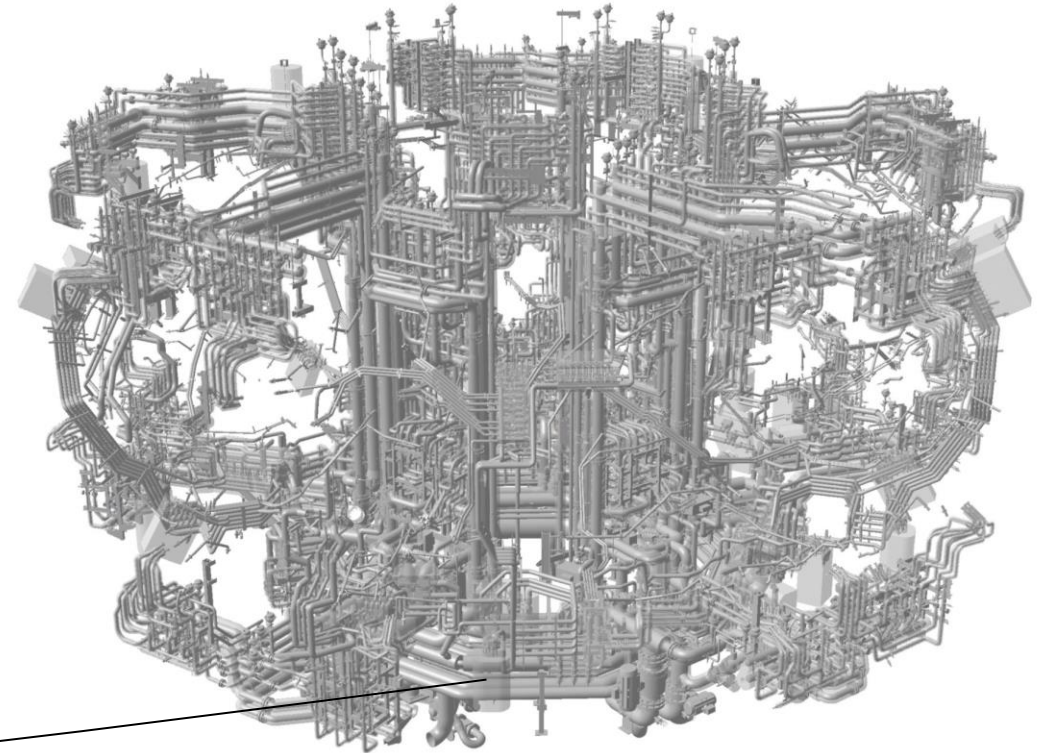
- First inspection after OP 2.1b
- Module 4, seen from M5First



Completion phase 2018-2020

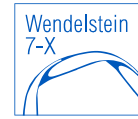


- 10 HHF Divertors
- 10 Cryo pumps with LHe
- complex cooling water system



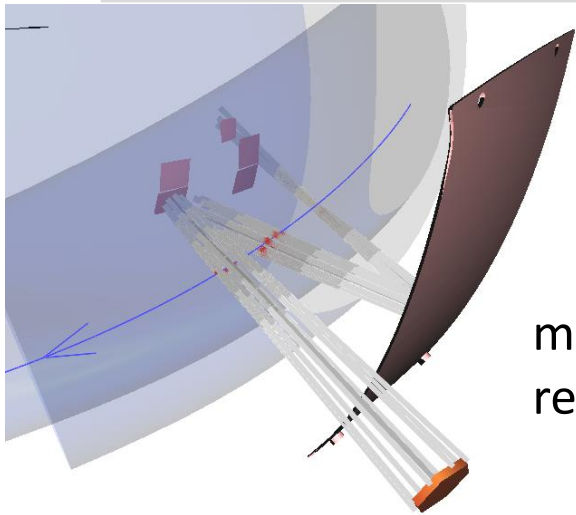
- pulse lengths up to 30 min possible
- full heating power
 - 10 MW ECRH, steady state
 - 10 MW NBI, for 10 s

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Electron cyclotron resonance heating above X2 cut-off



only 70% single beam O2 absorption (at 10^{20} m^{-3} and 3 keV)

multi-pass absorption/w reflection at tiles & panel

cut-off limits

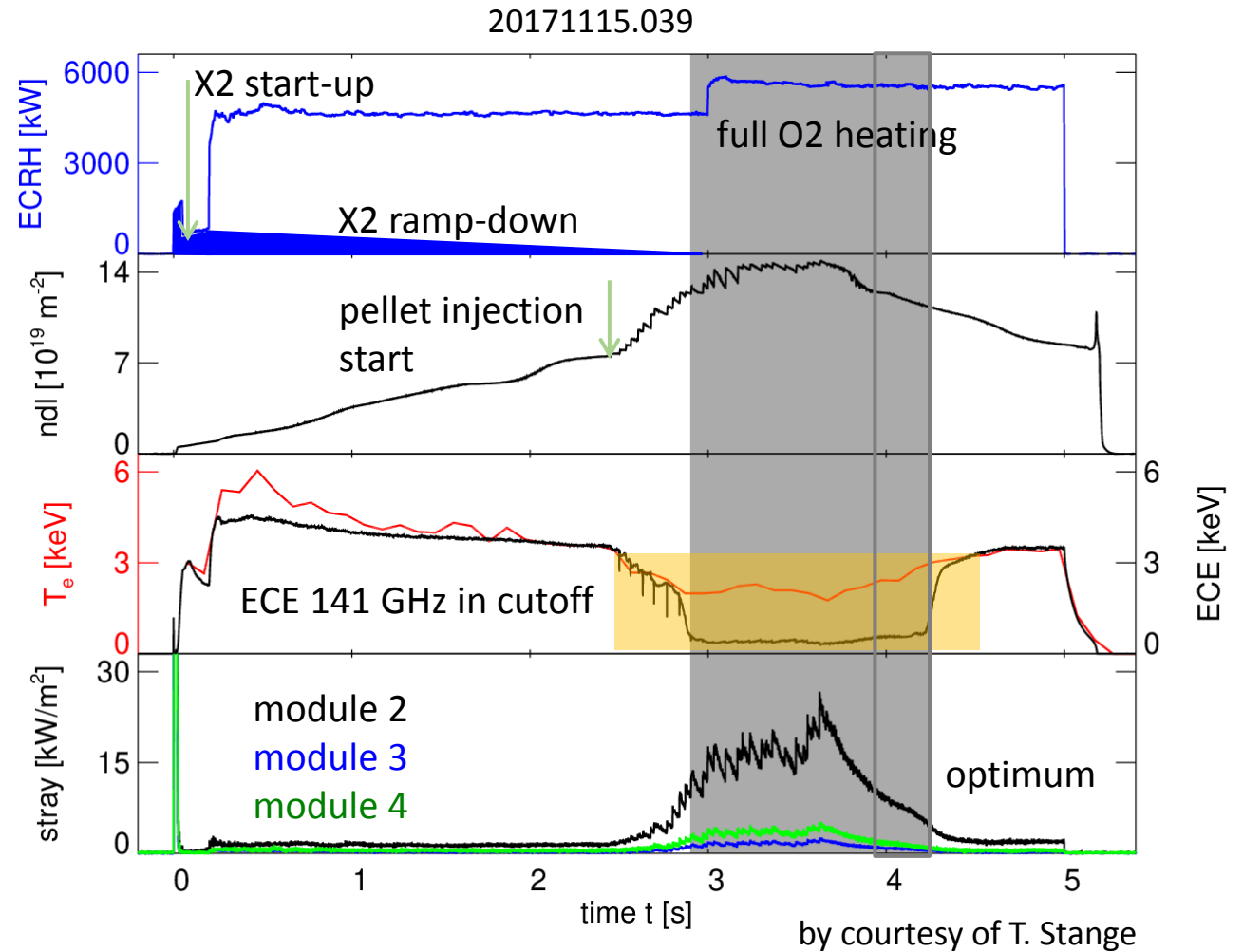
ECR X2 heating $n_e < 1.2 \cdot 10^{20} \text{ m}^{-3}$

ECR O2 heating $n_e < 2.4 \cdot 10^{20} \text{ m}^{-3}$

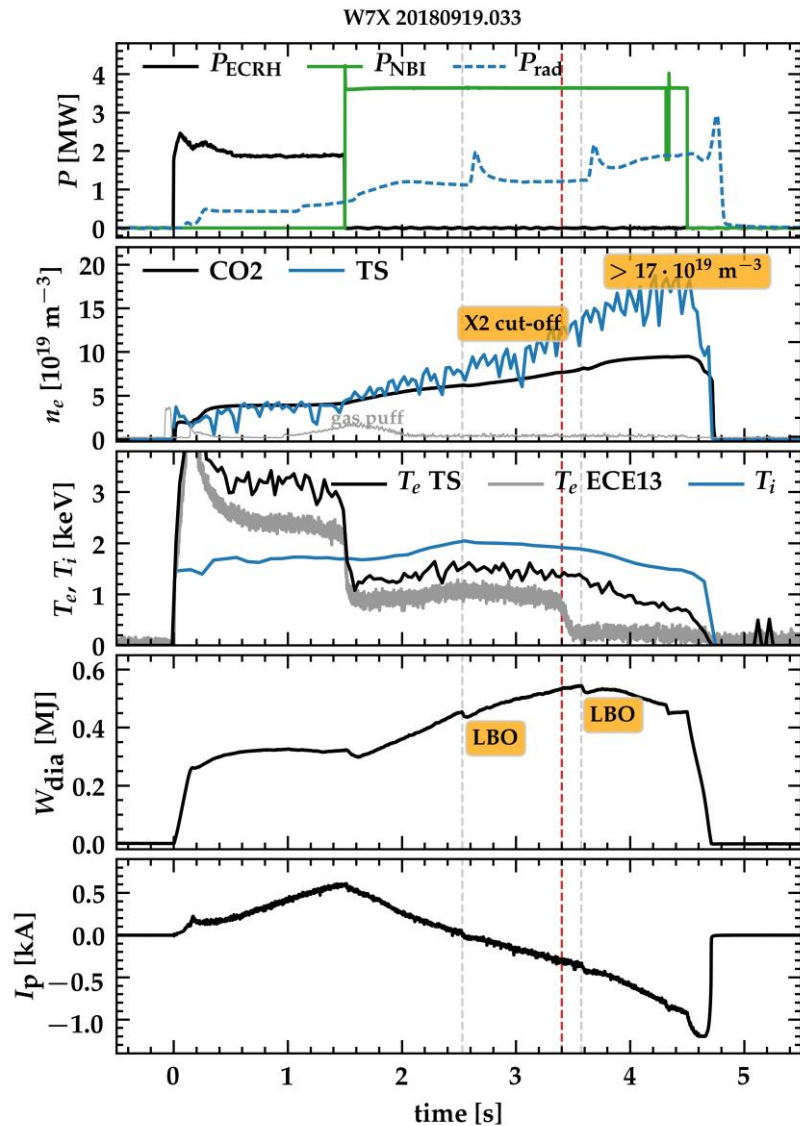
ECE and TS

stray radiation < 20 kW/m²

OXB mode conversion schemes under development

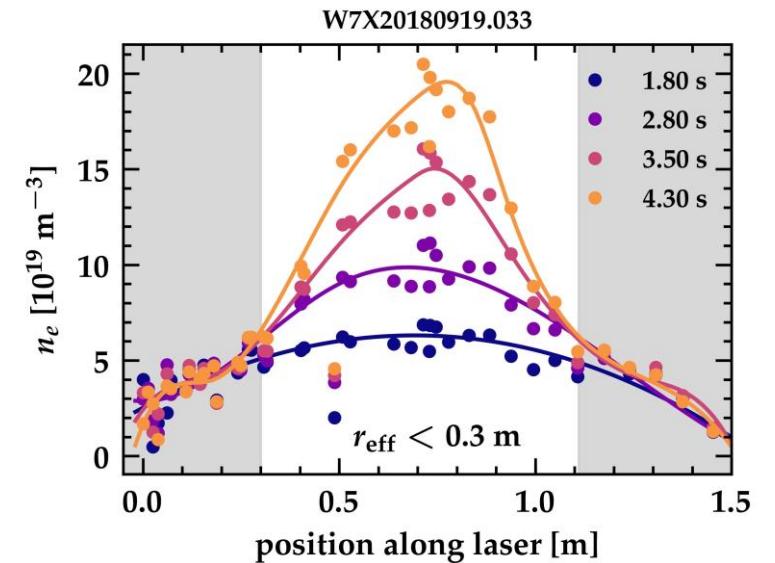


NBI heated discharges with high density



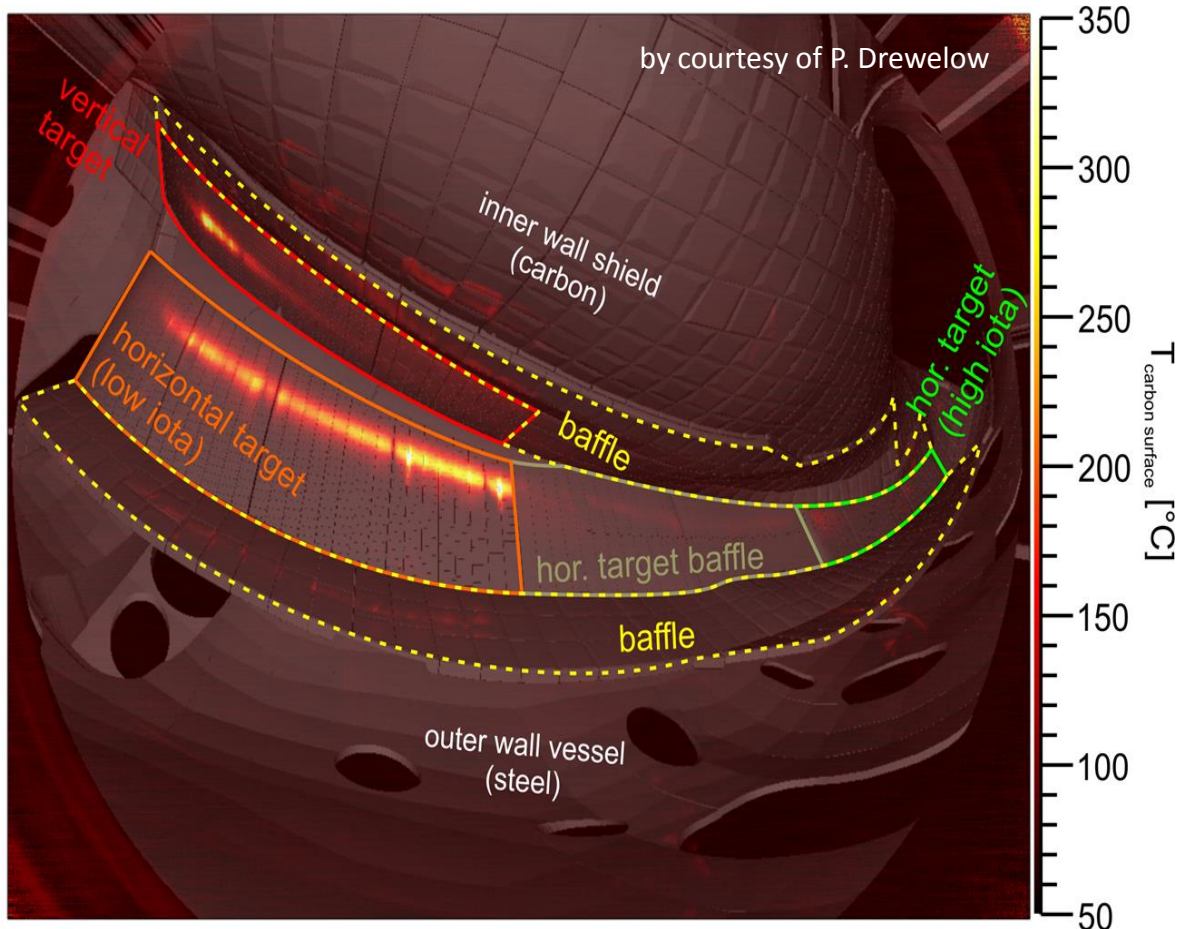
- pure NBI heating can sustain plasma
- stabilization of ion heating w/o ECRH

by courtesy of D. Hartmann



- centrally peaked high density plasma core
- density peaking can be controlled by additional ECRH
- pure NBI heating with $n_{\text{peak}}(0) = 2 \cdot 10^{20} \text{ m}^{-3}$ demonstrated

10 high resolution IR cameras

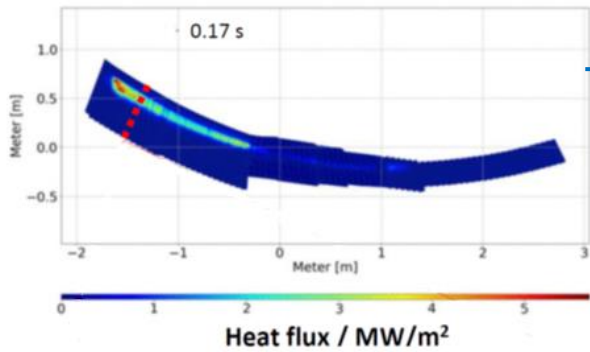


asymmetry toroidal $\leq 40 / 25\%$ (trim coils)
up/down $\sim 10\text{-}20\%$

power fall-off length $\lambda_q = 15 \dots 30 \text{ mm}$
power wetted area $A_{\text{wet}} \sim 1.2 \text{ m}^2$

strike lines defined by the long connection
lengths ranging between 200 m and 600 m

Power detachment

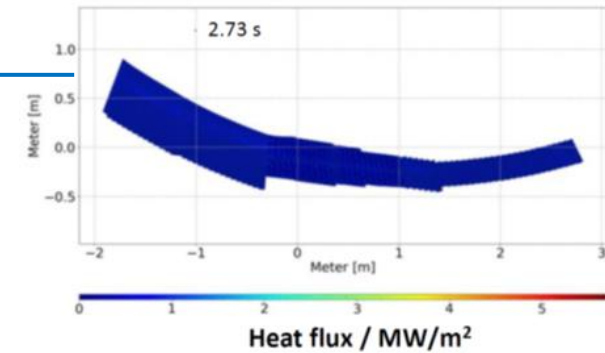
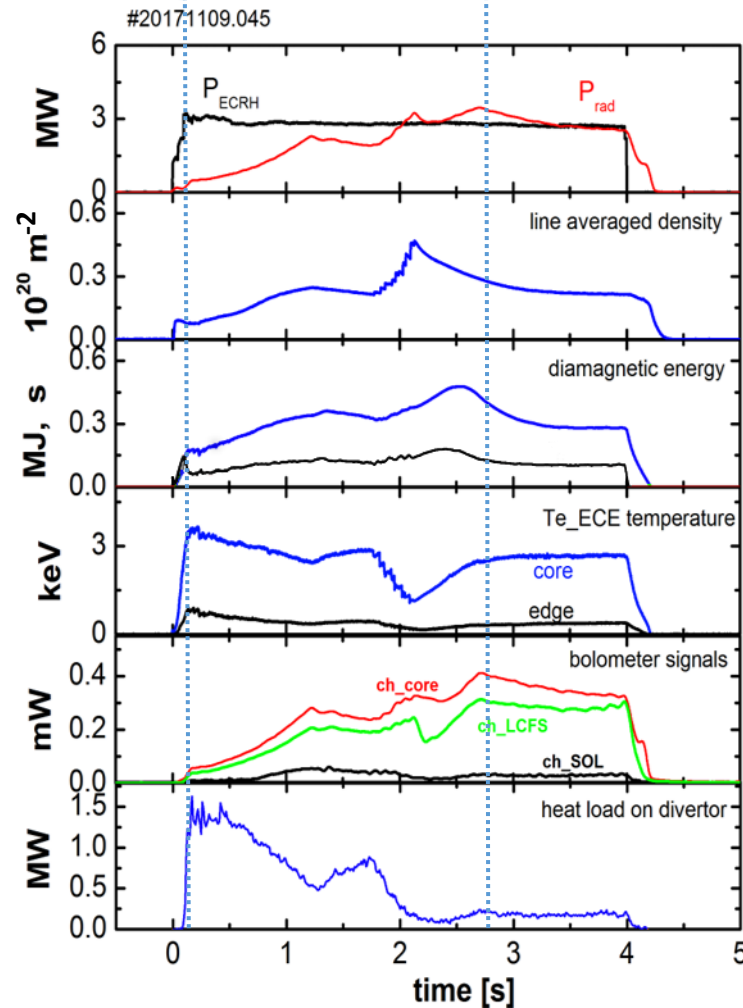


before detachment

H pellet injection into He
density ramp-up
to $4\text{-}5 \cdot 10^{19} \text{m}^{-2}$

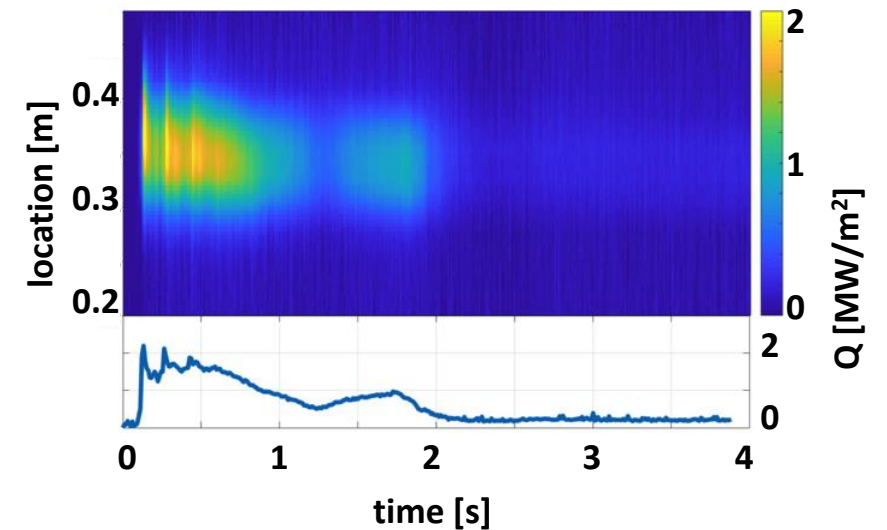
power load drops to \sim zero

detachment by pellet injection

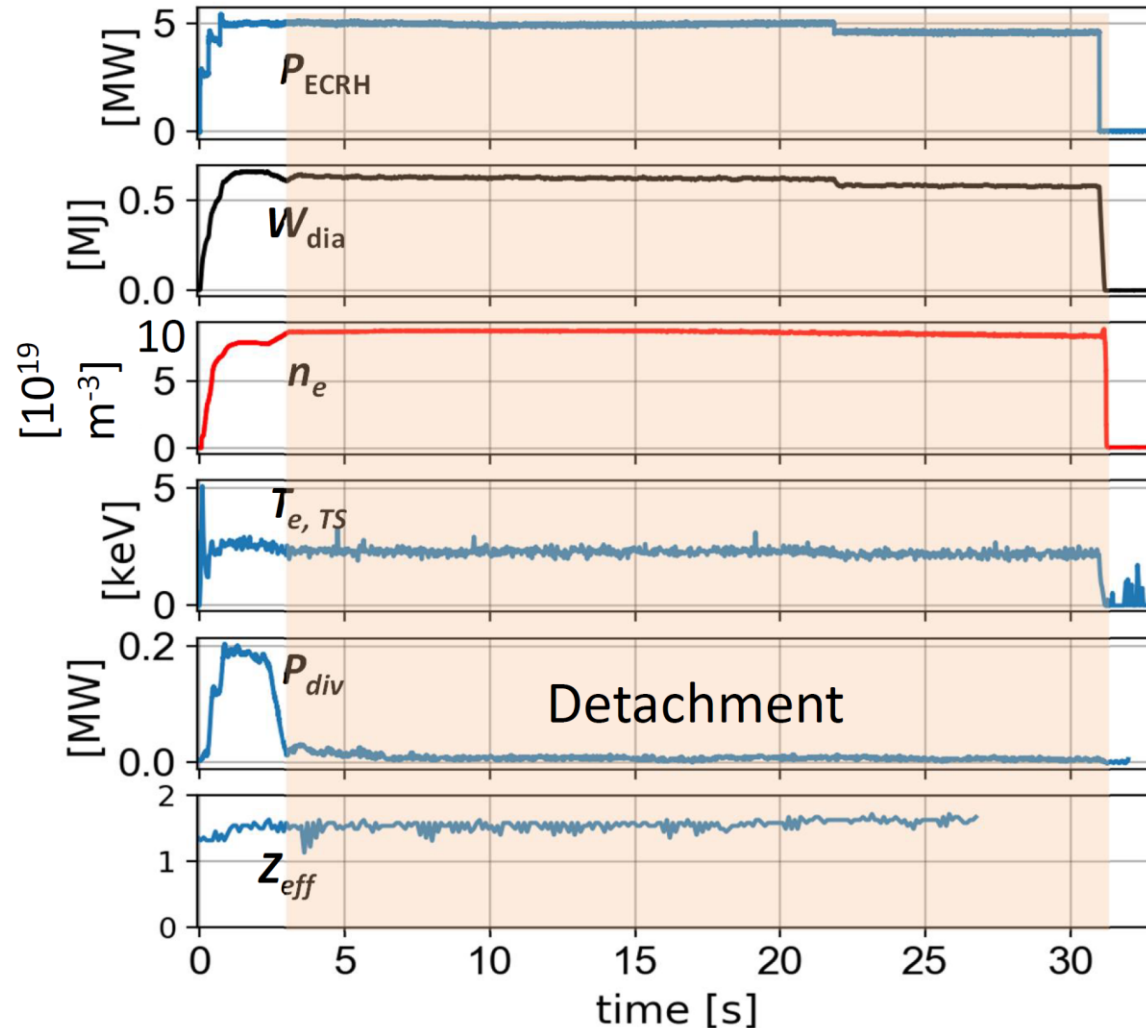


after detachment

time evolution of heat flux



Long pulse discharge with divertor detachment



02 ECR heating with 5 MW power 150 MJ

0.6 MJ diamagnetic energy $\tau_E \approx 0.1$ s

$0.9 \cdot 10^{20} \text{ m}^{-2}$ line-integrated density
30 s flat-top density feedback control

2.5 keV central electron/ion temperature

full detachment – div. pressure 0.07 Pa

Z_{eff} constant over the full discharge

reference scenario

A record high performance plasma

20171207.006

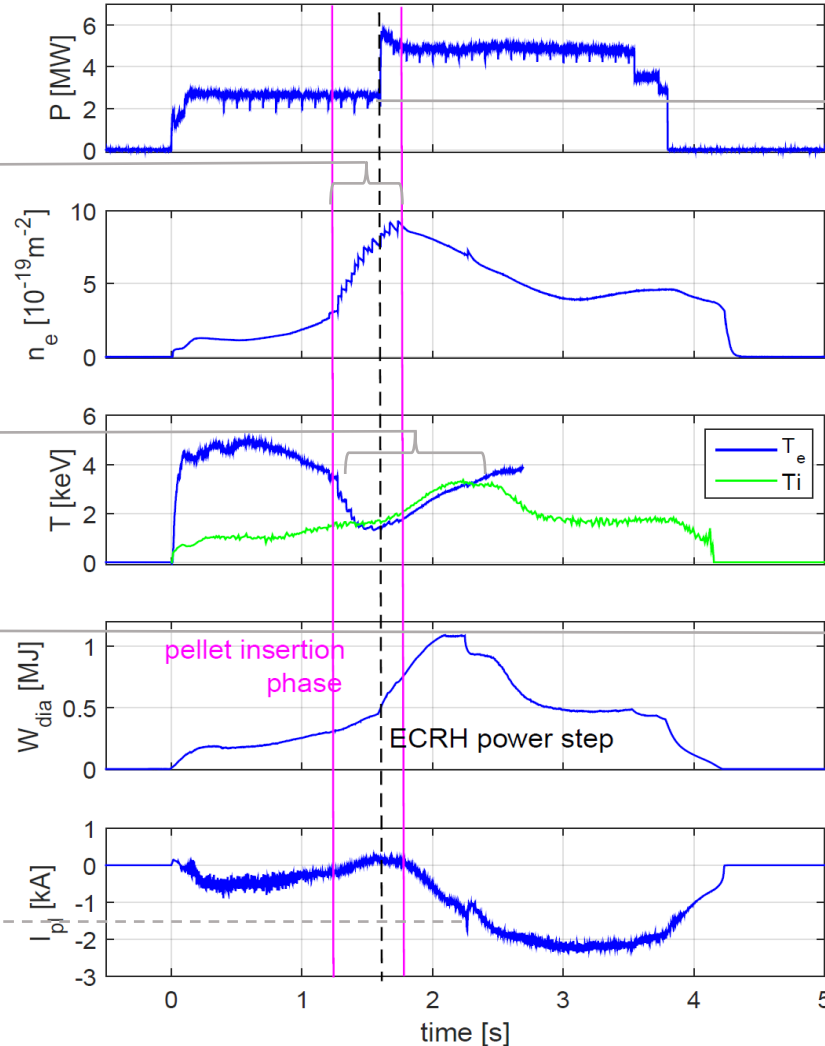
by courtesy of S. Bozhenkov

hydrogen pellet injection
into helium target plasma

thermalization $T_e = T_i$

diamagnetic energy ≥ 1 MJ

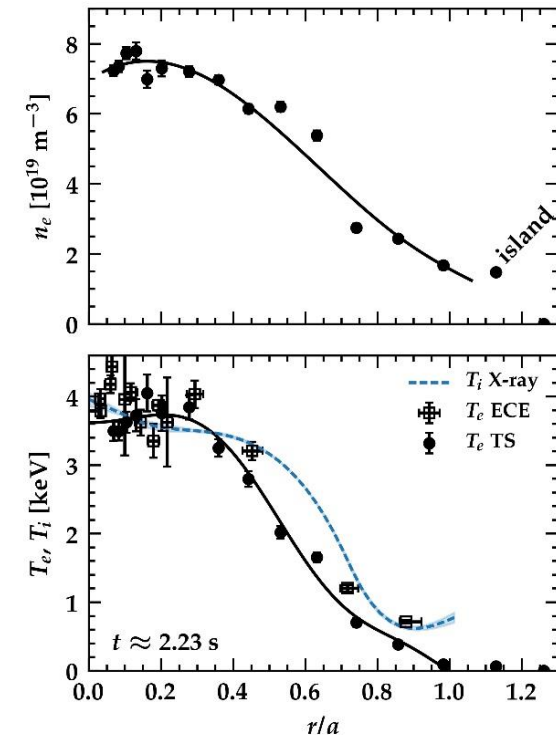
MHD event



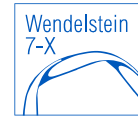
X2 ECRH power doubled

record triple product
 $\geq 0.6 \cdot 10^{20}$ keVs/m³

by courtesy of S. Bozhenkov



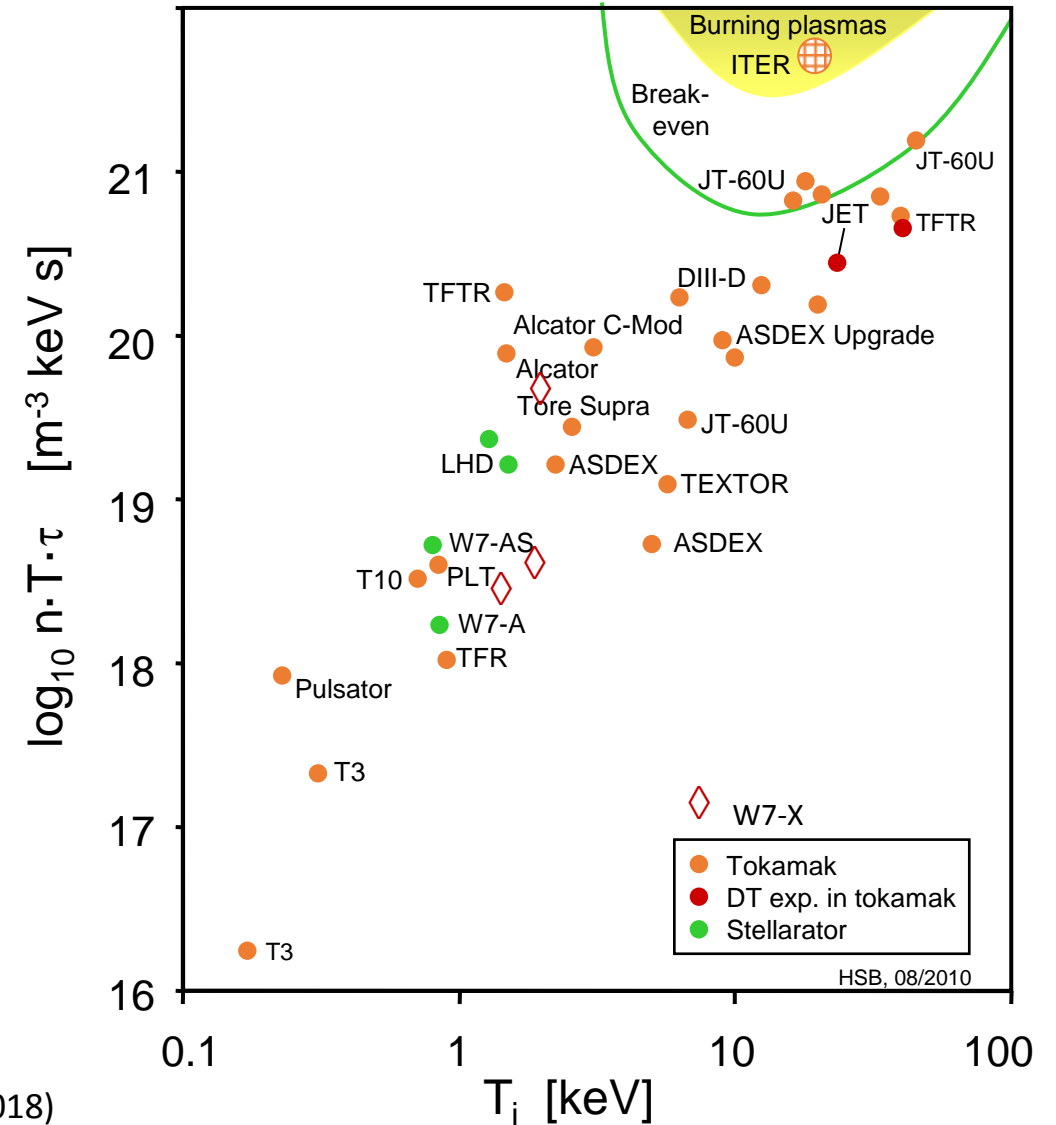
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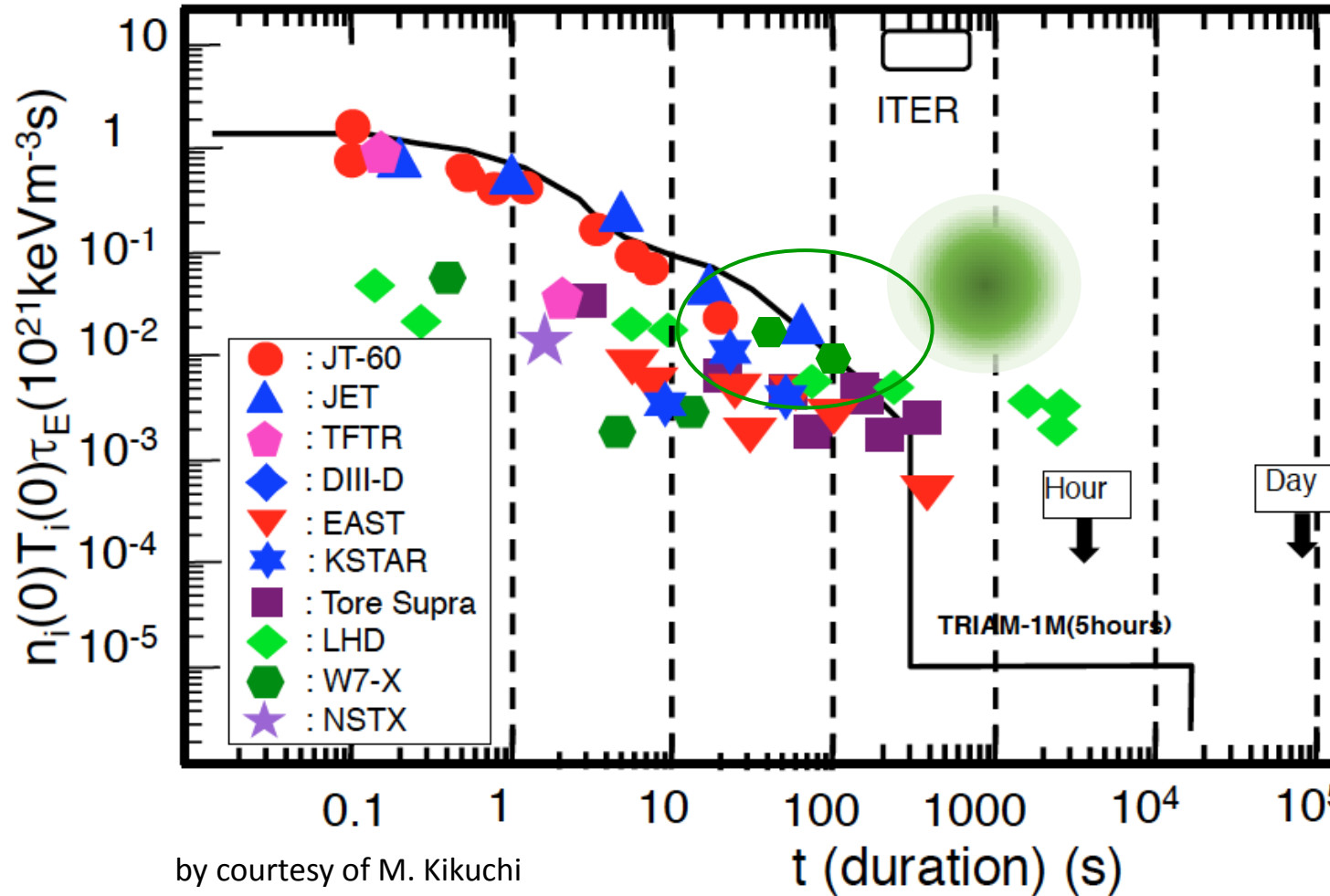
$nT\tau$ -diagram

- J. D. Lawson, 1957
- power balance for a fusion plasma
- 2 curves derived
- logarithmic scale
- a measure for the success of fusion
- factor 10^5 in 50 years
- However, most of these values are not stationary!

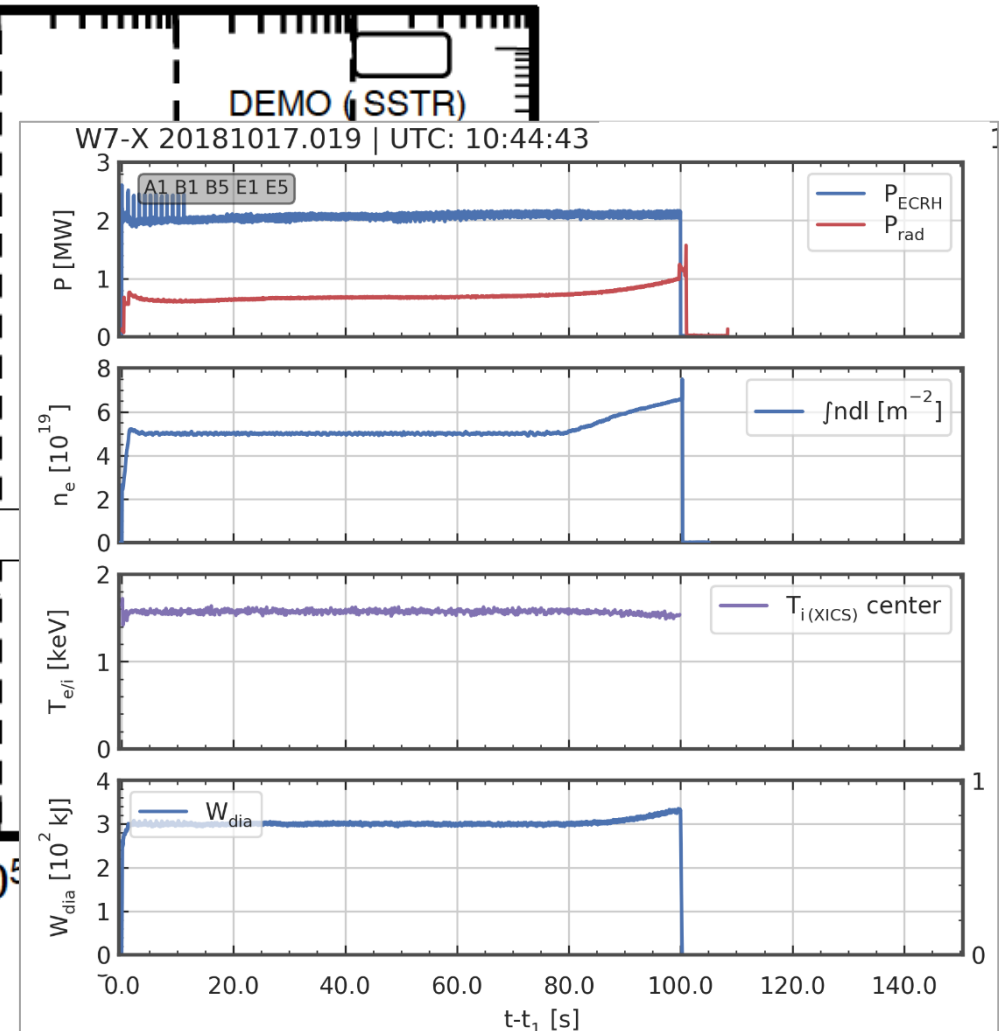


T.S. Pedersen, PPCF **61** (2018)

Fusion triple product and pulse length



by courtesy of M. Kikuchi
T.S. Pedersen, PPCF **61** (2018)

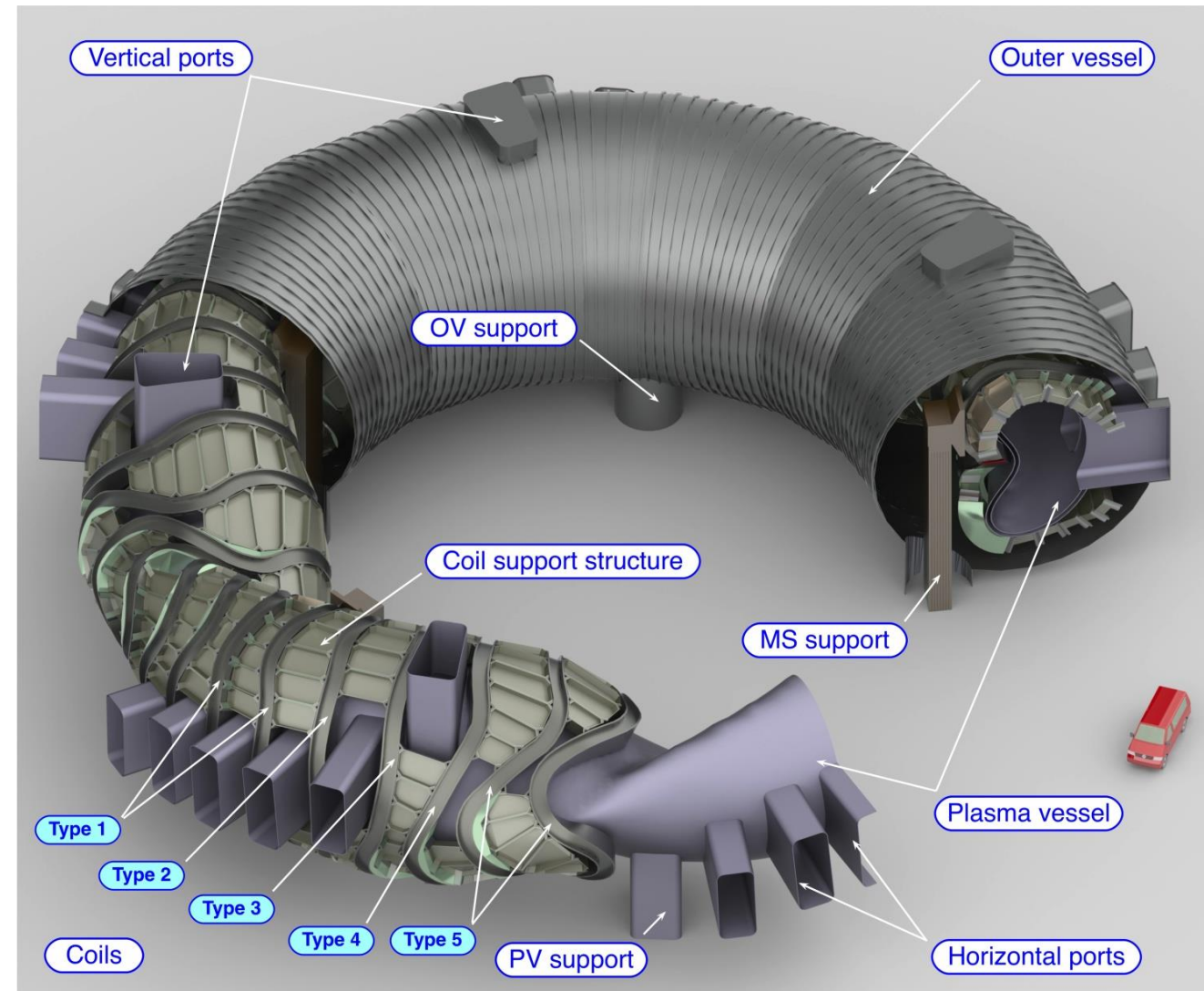


From W7-X to a HELIAS fusion power plant

Requirements / parameters

- Average magnetic field on axis 5 – 6 T (max. field at coils 10 – 12 T)
- Size of coils and magnetic field similar to ITER (ITER coils technology can be applied)
- Sufficient space for blanket (~1.3 m between plasma and coils)
- $\langle \beta \rangle = 4 - 5 \%$ (W7-X value!)
- Fusion power $\sim 3\text{GW}$
- Advantage of larger aspect ratio: Reduced neutron flux through wall (average 1 MW/m², maximum 1.6 MW/m²)

$$R = 22 \text{ m}, A = 12$$



Summary and conclusions



- 1. Fabrication and assembly of W7-X have been tedious, but the device turned out to be highly reliable and stable – it is easy to operate and mechanically stable.**
 - 2. The island divertor shows even heat load distribution, power detachment and discharges with controlled plasma radiation and high neutral compression rates.**
 - 3. Even before its completion, W7X has reached record nTt-values for helical devices.**
- Water cooling of all in-vessel components and active divertor pumping are now needed to further extend the discharge duration at high heating power.**
 - More ECRH heating power is needed and aimed for (perspective 12×1.5 MW).**